



Florida Bar Construction Law Committee

September 8, 2025

Champlain Towers South Collapse Investigation

Matthew Fadden, PhD, PE

*Managing Director and Principal
Walter P Moore Associates, Inc.*

Gary Klein, PE, SE

*Vice President and Senior Principal
Wiss, Janney, Elstner Associates, Inc.*

Presentation Outline

1. Champlain Towers South Collapse

Document Review

Site Investigation

Laboratory Studies

Structural Analyses



Collapse Theory



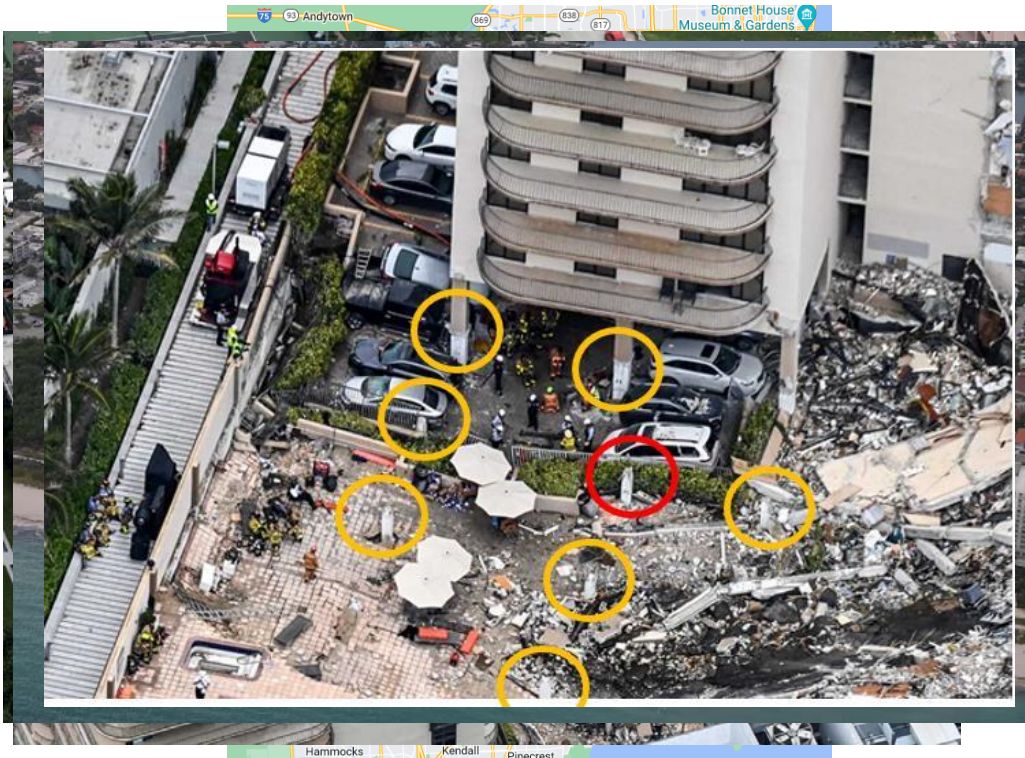
2. State of Structural Assessments in Florida

Findings & Observations

Document Review



What we knew June 24, 2021 – Surfside, FL



- A building had partially collapsed at ~1:30 am
- 100+ people were feared missing or dead
- The cause was unclear
- Initial information via:
 - Social media
 - News
 - Photos
 - Videos

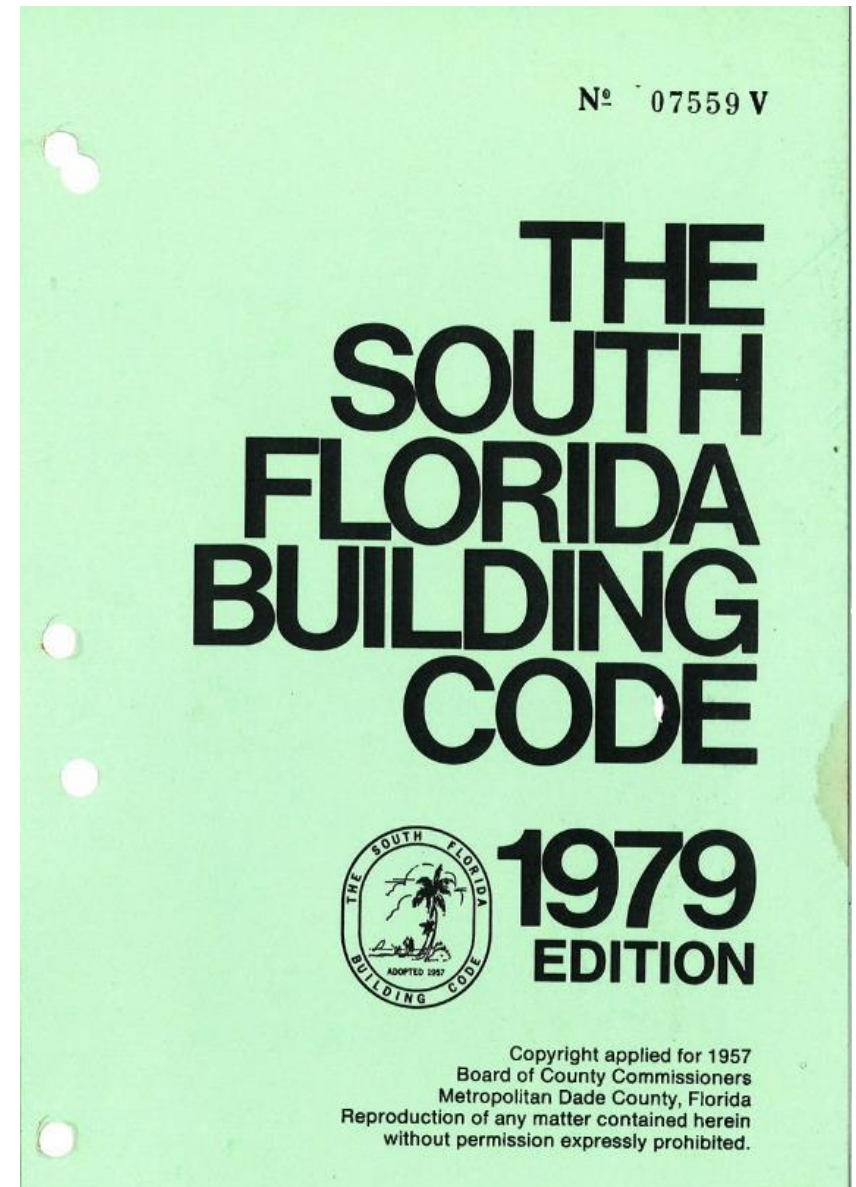
Building Description

- 12-story L-shaped structure with 136 units built in 1981
- Reinforced concrete flat plate construction
- Parking on the lobby level and the basement garage
- Pool deck terrace on the south side of the buildings



Codes and Design Standards (1981)

- South Florida Building Code 1979
- ACI 318-77: Building Code Requirements for Reinforced Concrete



NOTE:
ALL PLANTING AREAS TO
HAVE TOPSOIL WATERPROOFING
AND DRAINAGE HOLES
WHERE PLANTING

North

Collins Ave.

K/13.1

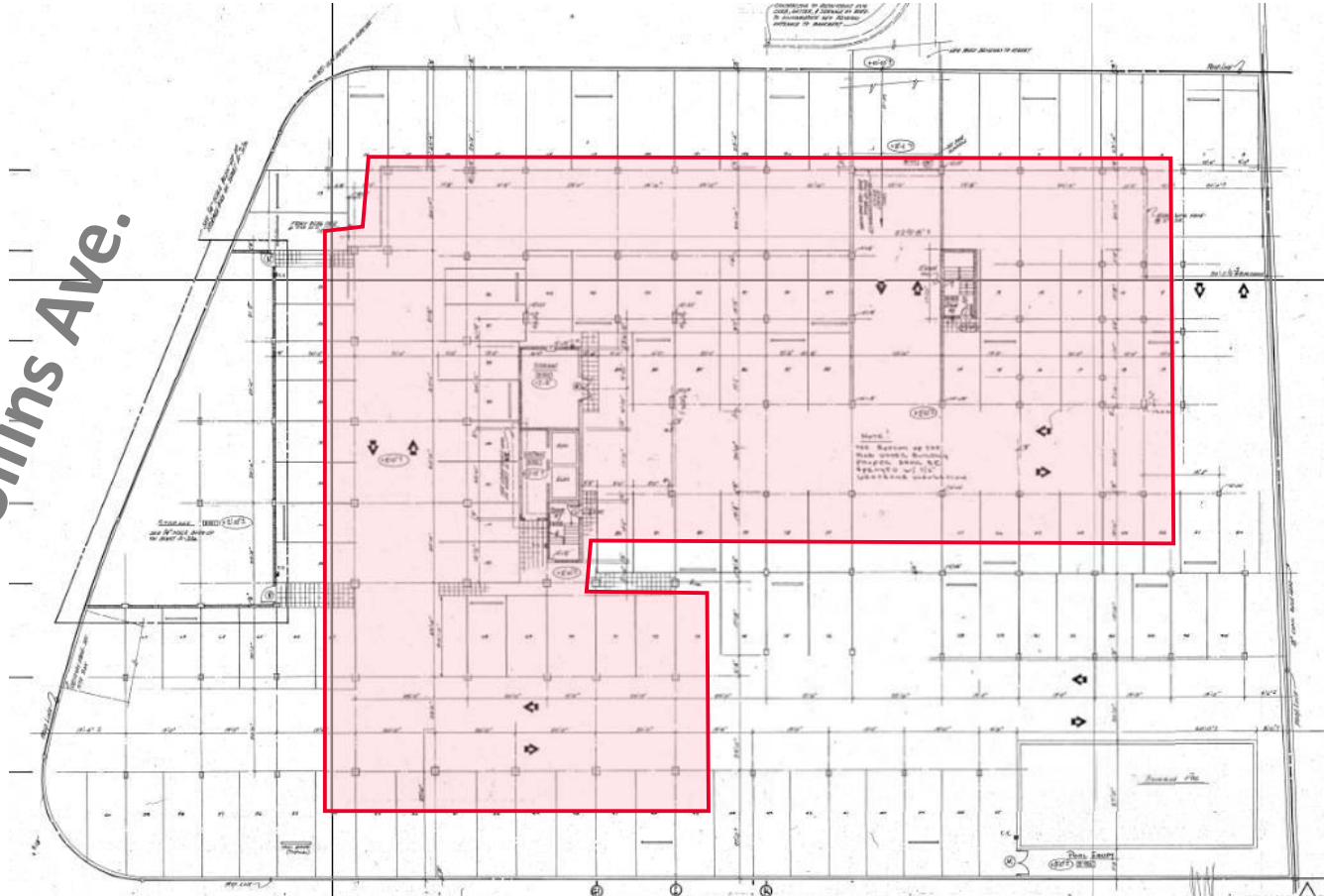
L/13.1

Atlantic Ocean

North



Collins Ave.

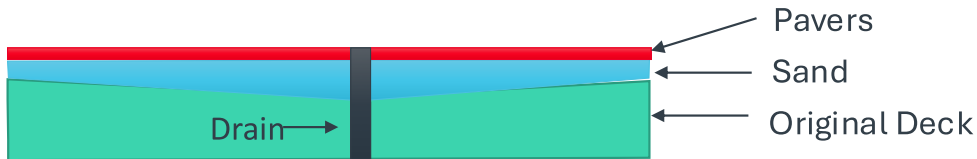


Atlantic Ocean

1996 Retrofit: Pool Deck & Garage

Under the supervision of a licensed Florida professional engineer, a repair contractor performed:

- Planter waterproofing
- Paver installation
- Concrete structural repairs



March 22, 1996

Thomas Conway
Building Manager
Town of Surfside
9293 Harding Avenue
Surfside, FL 33154

Dear Mr. Conway,

██████████ will be starting a project at Champlain Towers South located at 8777 Collins Avenue, Surfside FL. Included in the scope of work will be concrete structural repair in the parking garage. This type of repair entails removing loose concrete overhead, treating steel rebar with rust inhibitive coating and patching back with repair mortar. Also included in the garage will be urethane foam injection in ceiling cracks (approximately 500 lineal ft.).

The condo has retained the services of ██████████ 5100 West Copans Road, Margate, FL 33063 to do the inspections and supervise the project.

Please feel free to contact me with any questions.

Sincerely,

██████████
Sales Manager

2018 Recertification Report

- Abundant cracking and spalling in garage with calcium carbonate leaching
- Previous repairs failing due to poor workmanship
- Concrete repair recommended following standard practices
- Recommend that the entrance and pool decks slabs showing distress be removed and replaced



Figure J1: Typical cracking and spalling at parking garage columns



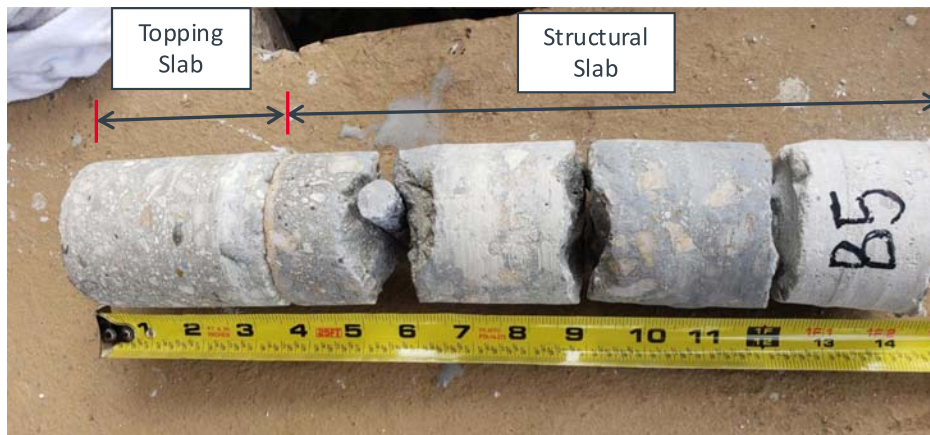
Figure J2: Spalling with exposed steel reinforcement at topside of garage deck.

Recertification Investigation – Deck Finish

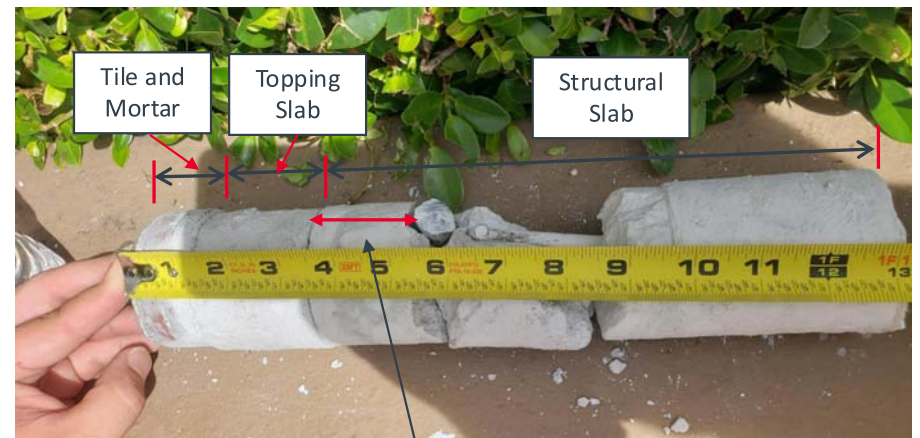


Recertification Investigation – Concrete Core Samples

Parking Deck

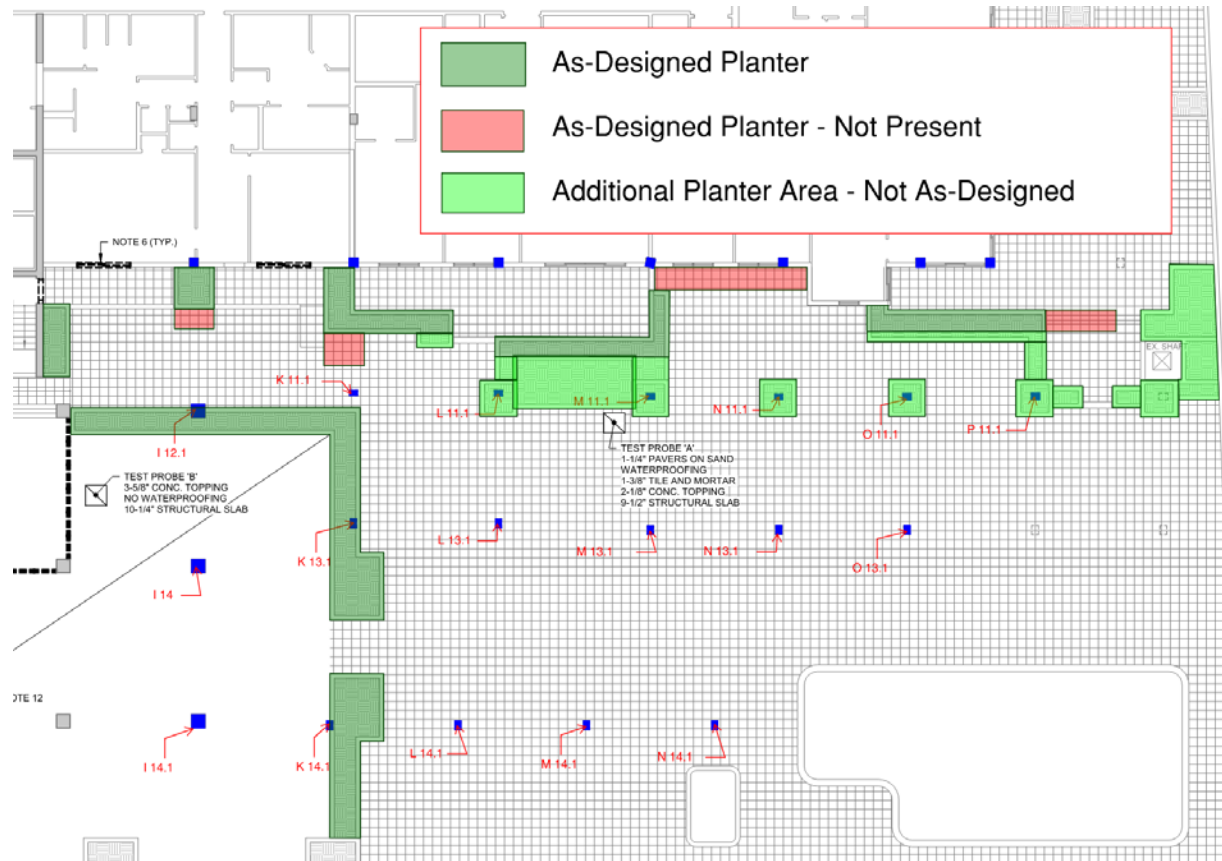


Pool Deck



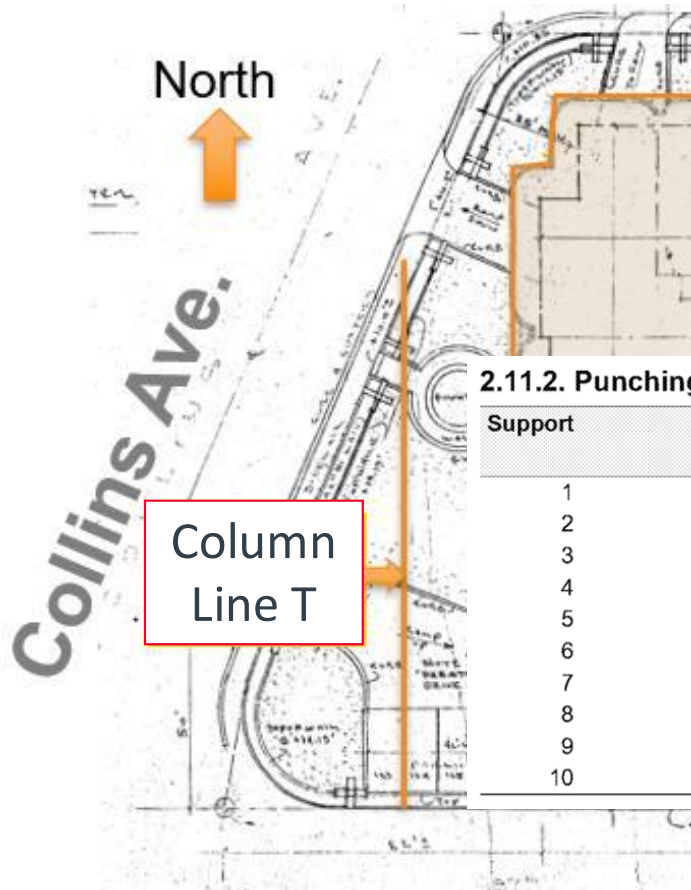
Excessive Cover

Recertification Investigation - Planters



Recertification Engineer Calculations

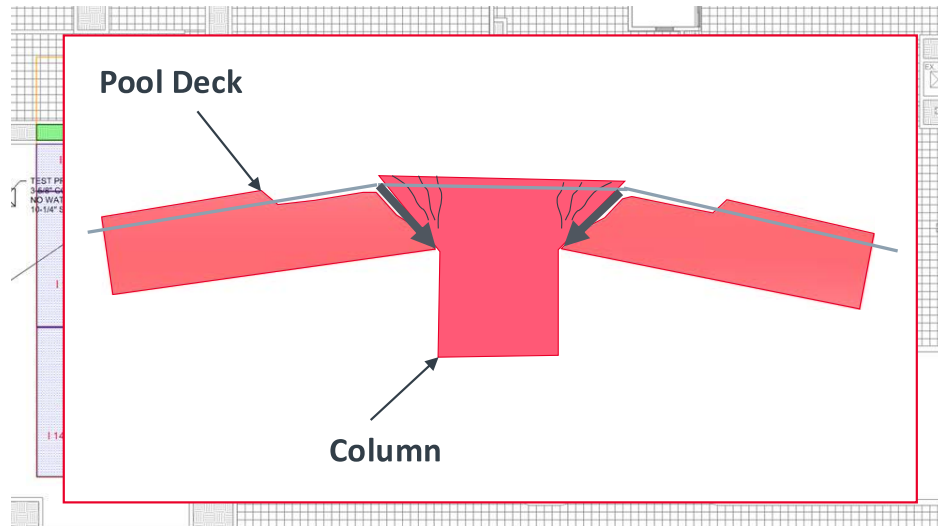
- Recertification engineer analyzed the slab along Column Line T
- Punching shear results were exceeded in every calculation iteration.



2.11.2. Punching Shear Results

| Support | V_u kip | v_u psi | M_{unb} k-ft | Comb | Patt | γ_v | v_u psi | ΦV_c psi |
|---------|--------------|--------------|-------------------|------|------|------------|--------------|-------------------|
| 1 | 80.05 | 31.9 | 195.51 | U1 | All | 0.117 | 343.7 | 101.5 *EXCEEDED |
| 2 | 202.56 | 236.6 | 10.47 | U1 | All | 0.415 | 244.8 | 189.7 *EXCEEDED |
| 3 | 133.15 | 183.2 | -39.19 | U1 | All | 0.422 | 217.6 | 189.7 *EXCEEDED |
| 4 | 164.83 | 192.5 | 12.83 | U1 | All | 0.375 | 200.5 | 189.7 *EXCEEDED |
| 5 | 176.45 | 206.1 | -18.39 | U1 | All | 0.415 | 217.8 | 189.7 *EXCEEDED |
| 6 | 133.61 | 183.9 | 6.98 | U1 | All | 0.422 | 190.0 | 189.7 *EXCEEDED |
| 7 | 156.94 | 216.0 | 6.70 | U1 | All | 0.422 | 221.8 | 189.7 *EXCEEDED |
| 8 | 146.79 | 171.5 | -25.71 | U1 | All | 0.375 | 191.2 | 189.7 *EXCEEDED |
| 9 | 178.11 | 180.7 | 16.77 | U1 | All | 0.380 | 190.3 | 189.7 *EXCEEDED |
| 10 | 77.04 | 30.7 | -172.04 | U1 | All | 0.117 | 299.8 | 101.5 *EXCEEDED |

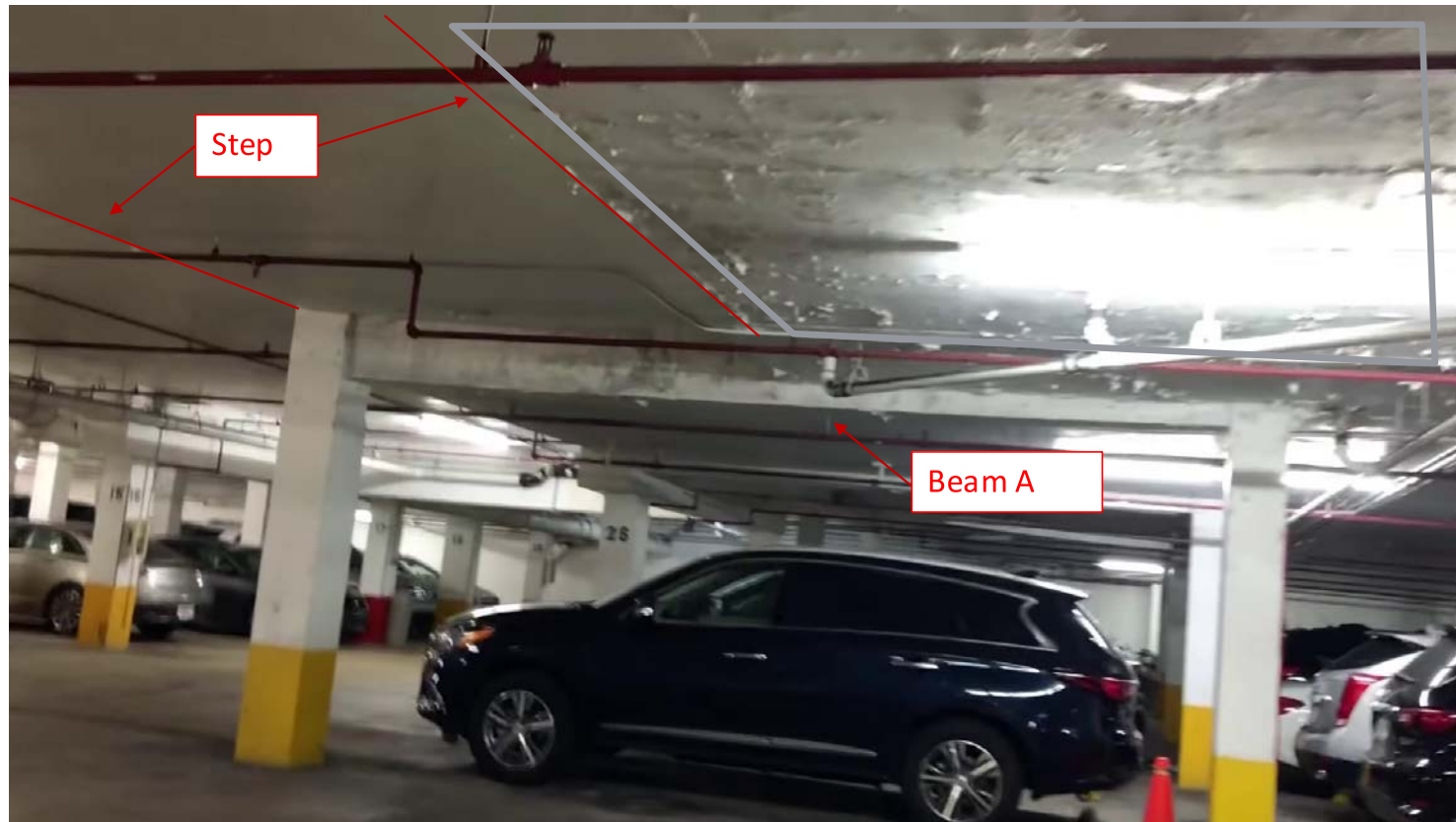
L13.1 Slab/Column Distress – Nov. 13, 2020



K13.1 Slab/Planter Distress - June 2, 2021



Garage Walkthrough Video



1:18 AM - TikTok Video



~1:15-1:22 AM - Unit 711 Ring Video



Resident Observations



Unit 711

Ring Video

Unit 611

Cracks in Walls

Unit 111

12:30 am:
Construction Noises
1:10-1:15 am:
Pool Deck Collapse



**Collapse Timeline
June 24, 2021**

| | | |
|----------------|--------------------------------|------------------|
| 1 | 1:10– 1:15 AM | Pool Deck |
| 7 – 12 minutes | | |
| 2 | 1:22 AM | East Tower South |
| 3 | + 3 seconds | East Tower North |
| 4 | + 8 seconds | East Tower East |
| 5 | West portion does not collapse | |



Findings & Observations

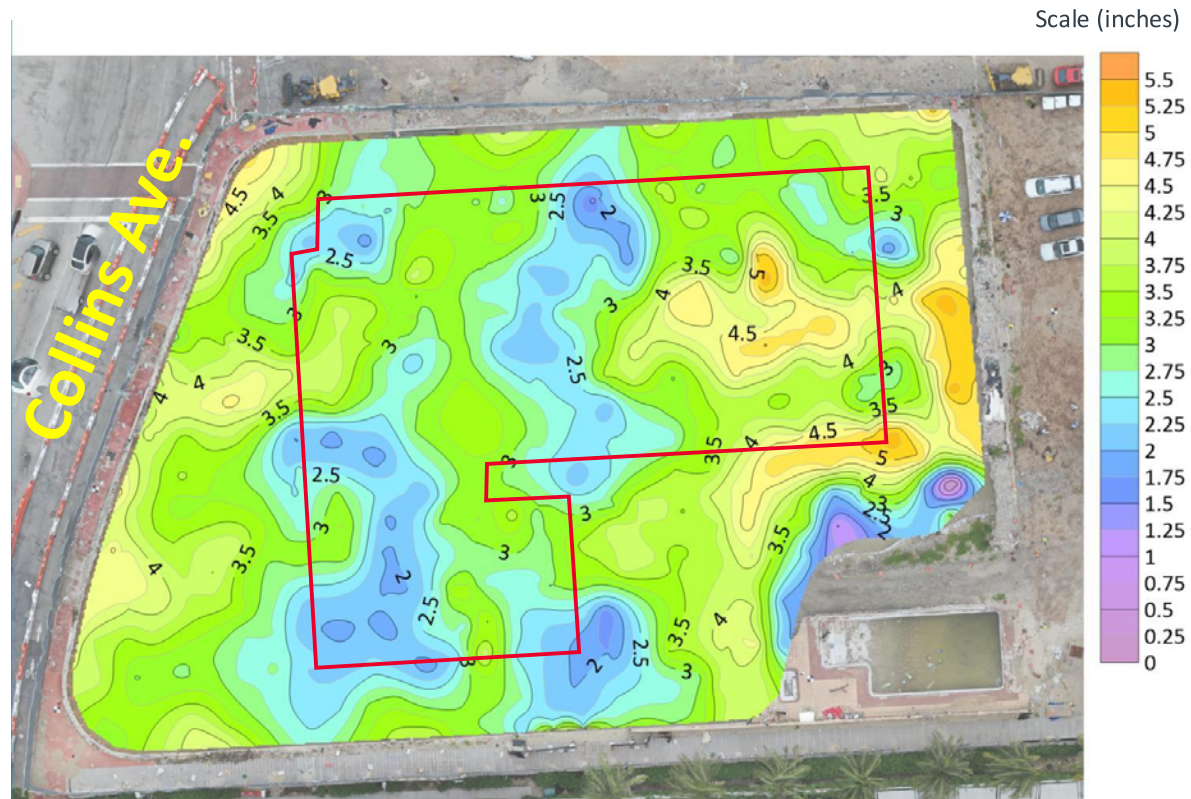
Site Investigation



Collapse Site – October 2021



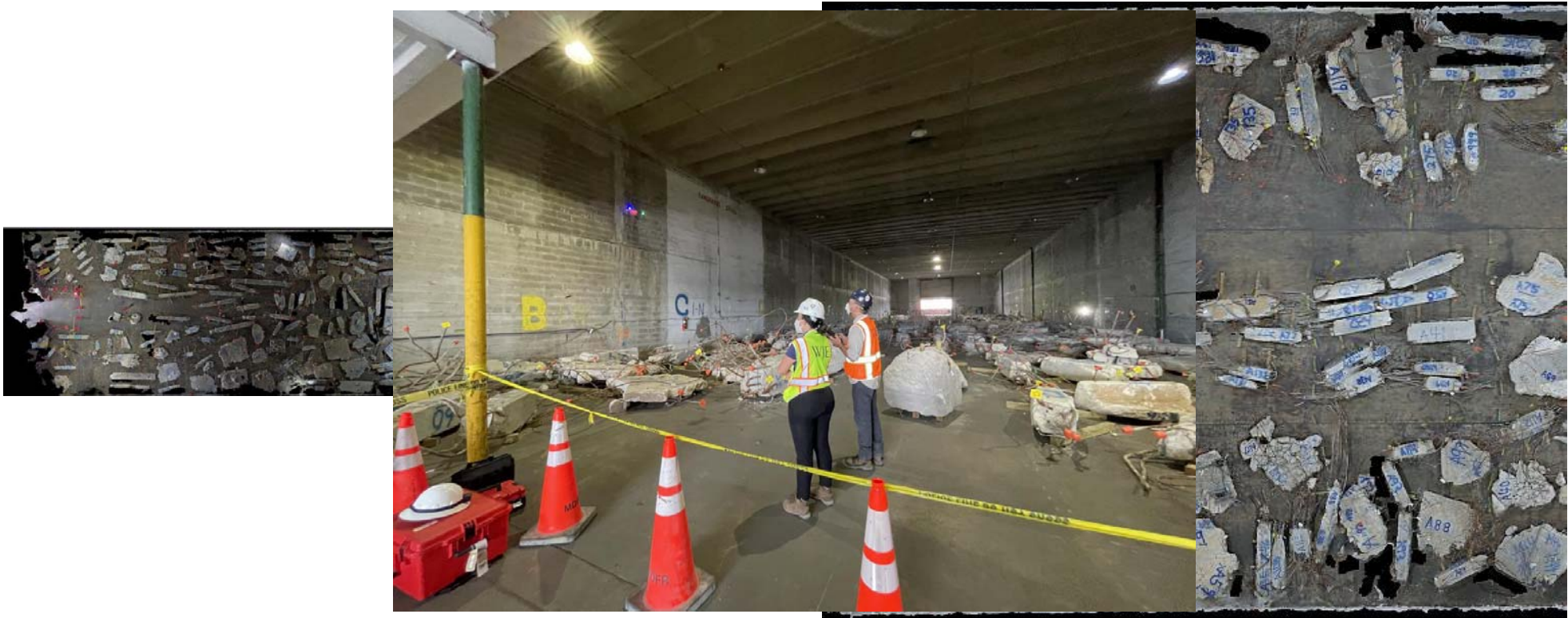
Basement Slab Survey - Topography



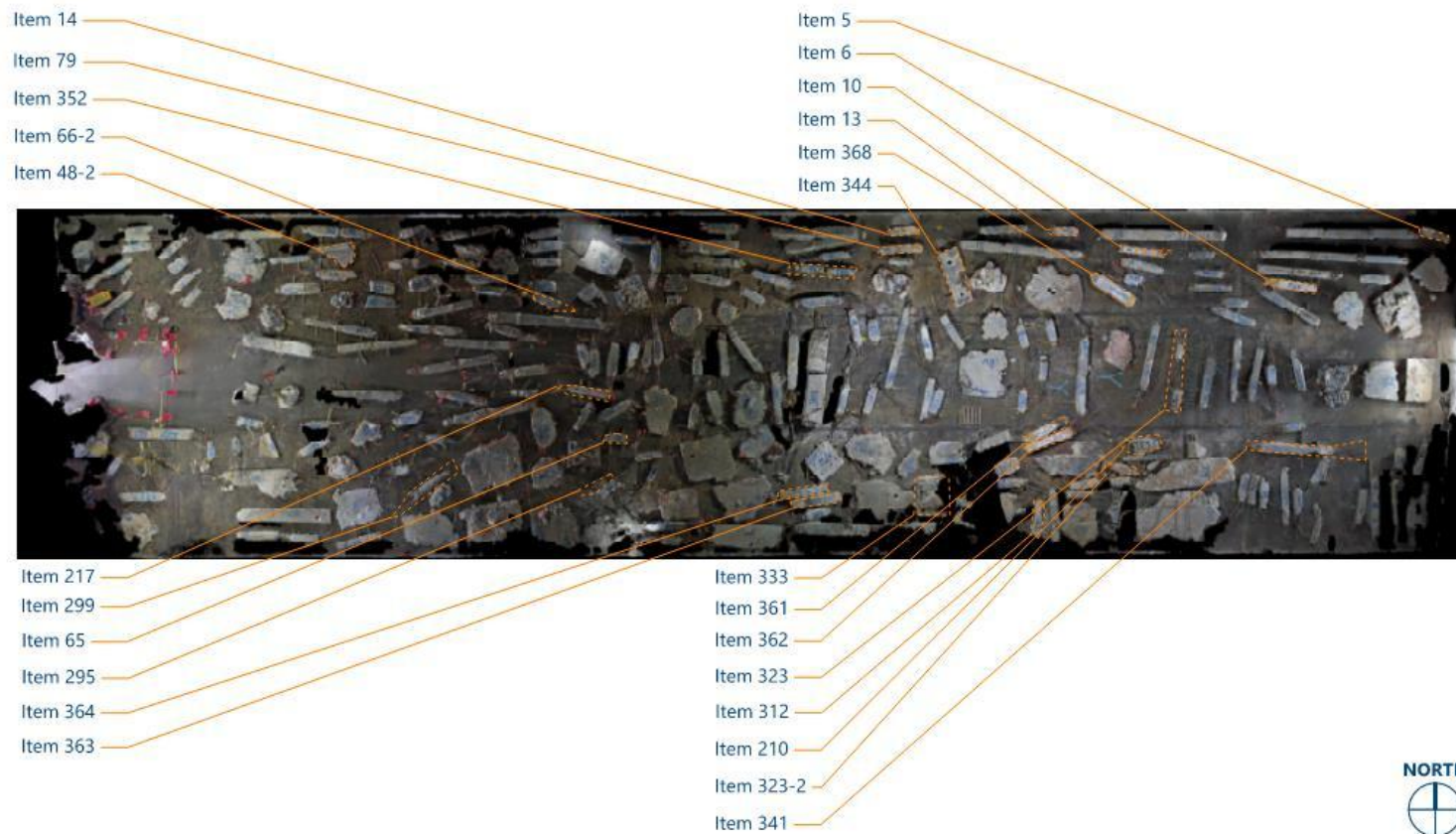
Collapse Site Sampling



NIST/NCST - Primary Evidence Facility



Primary Evidence Facility – North Bay*



Primary Evidence Facility – South Bay

Majority of Items from
Collapsed Portion

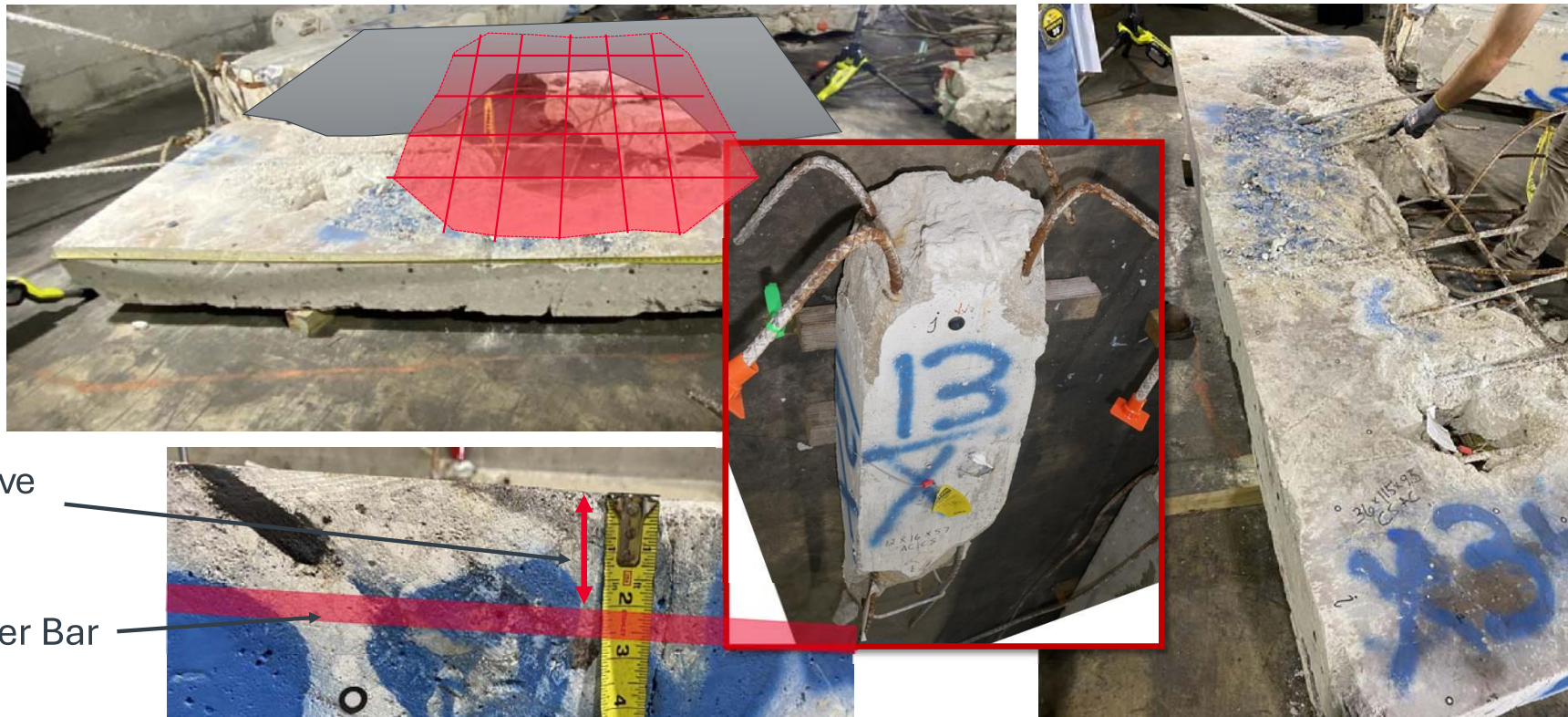
Item 119
Item 128
Item 68
Item 999



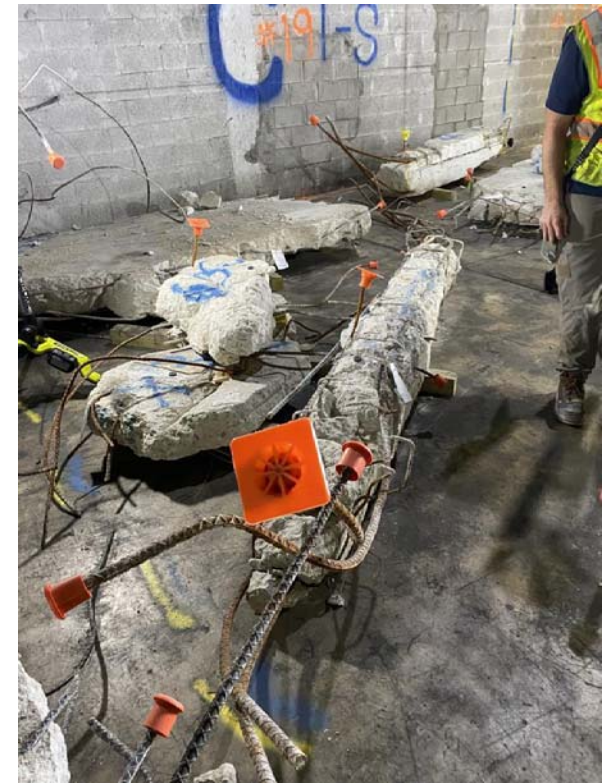
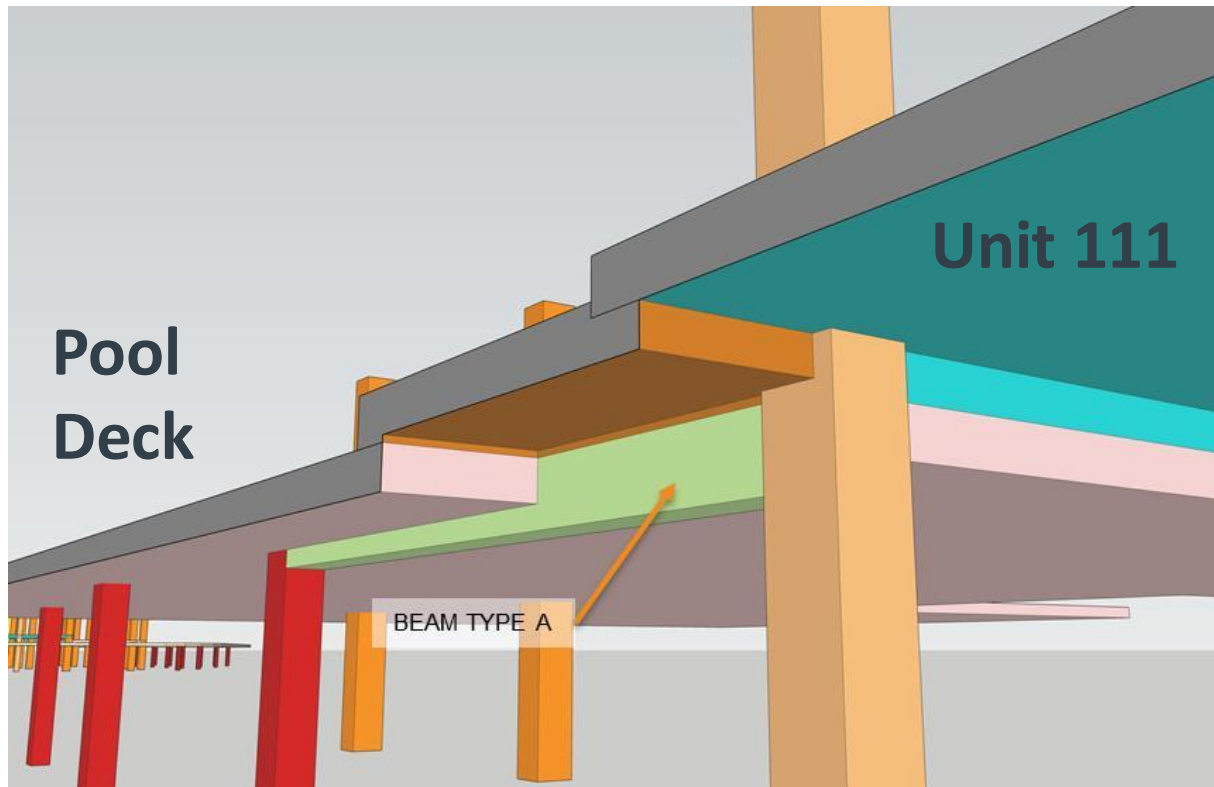
Majority of Items from
Imploded Portion



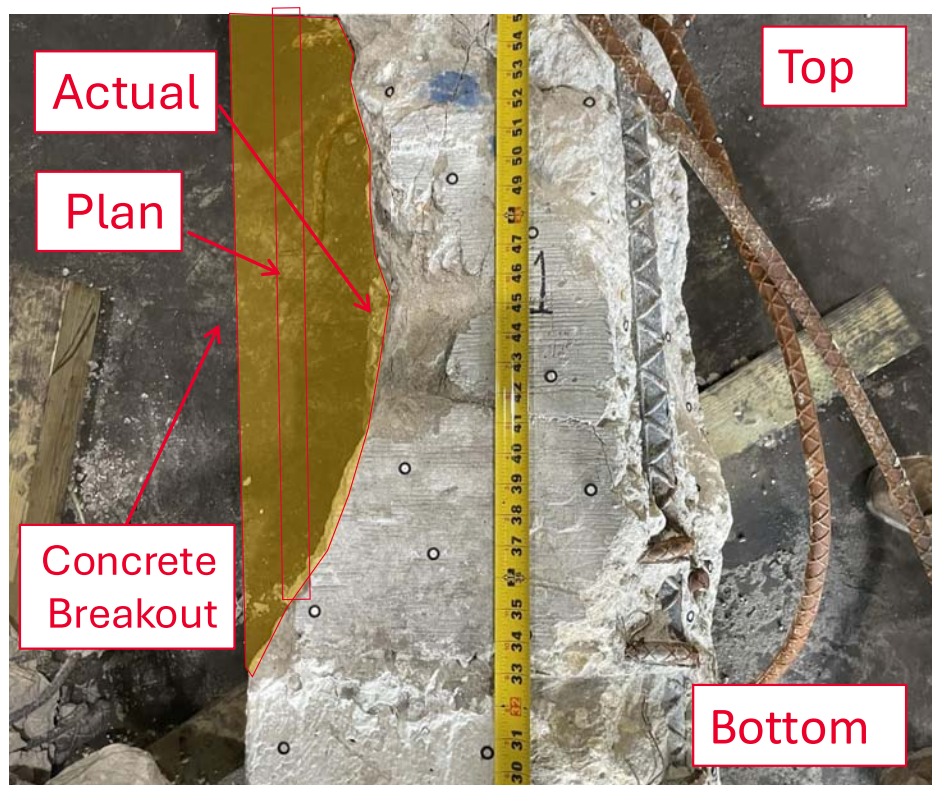
Primary Evidence Facility – Item 344 "Punched Slab"



PEF – Item 299 "Beam A"



Primary Evidence Facility – Item 341 - 16x16 Column

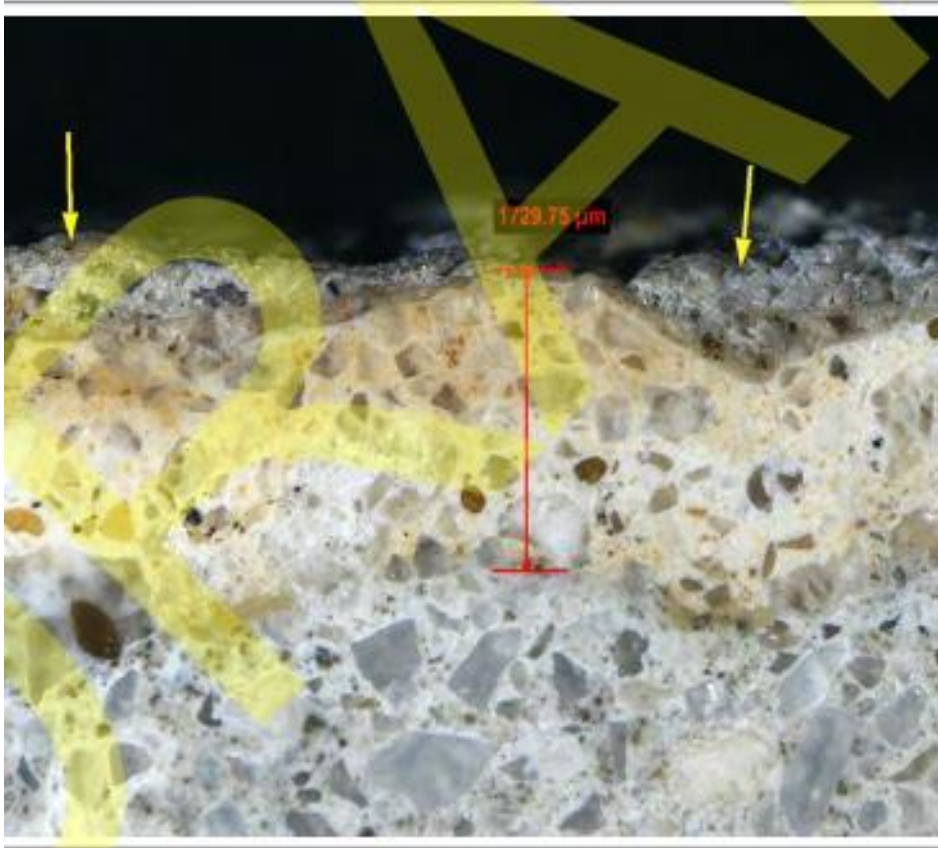


Findings & Observations

Laboratory Studies



Concrete Petrography and Testing

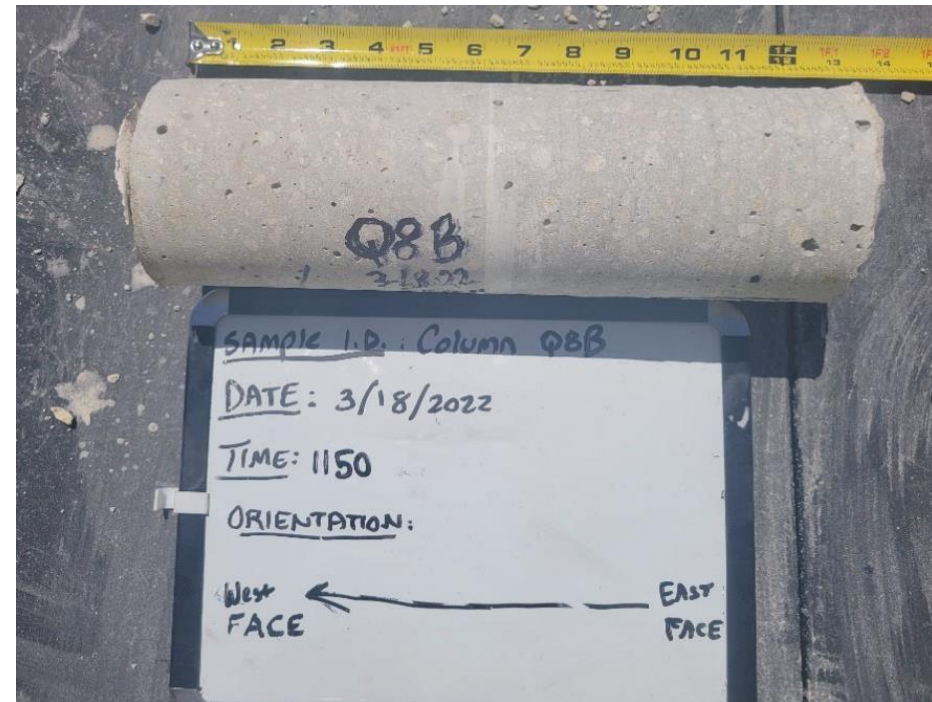


Basement Slab Samples

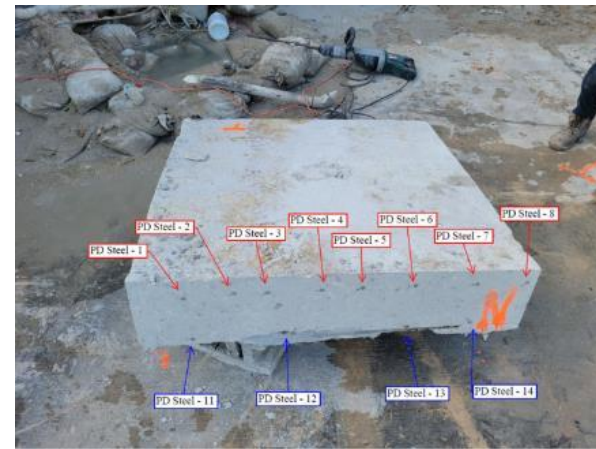
- Concrete typical to Florida
 - Moderate w/c ratio (0.35-0.45)
 - Well mixed
 - Non-air entrained
- Corrosion consistent with that at concrete placement
- Low chlorides and carbonation

Concrete Material Properties

| Location | Average Compressive Strength psi (MPa) | Min. Specified Compressive Strength psi (MPa) |
|-----------------|---|--|
| Transfer Girder | 3560 (25) | 4000 (28) |
| Column M15.1 | 3785 (26) | 6000 (41) |
| Column Q8 | 5820 (40) | 6000 (41) |
| Pool Deck | 4475 (31) | 4000 (28) |
| Perimeter Wall | 4280 (30) | 4000 (28) |
| Shear Wall East | 6600 (46) | 6000 (41) |
| Shear Wall West | 8155 (56) | 6000 (41) |



Steel Reinforcement



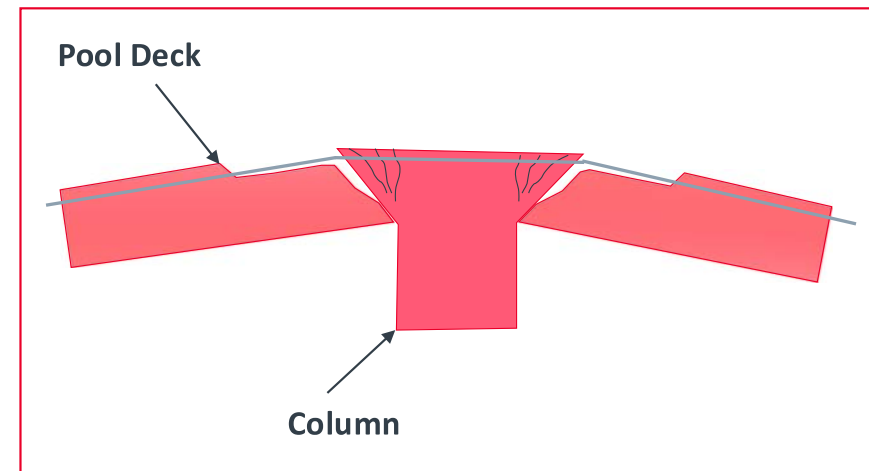
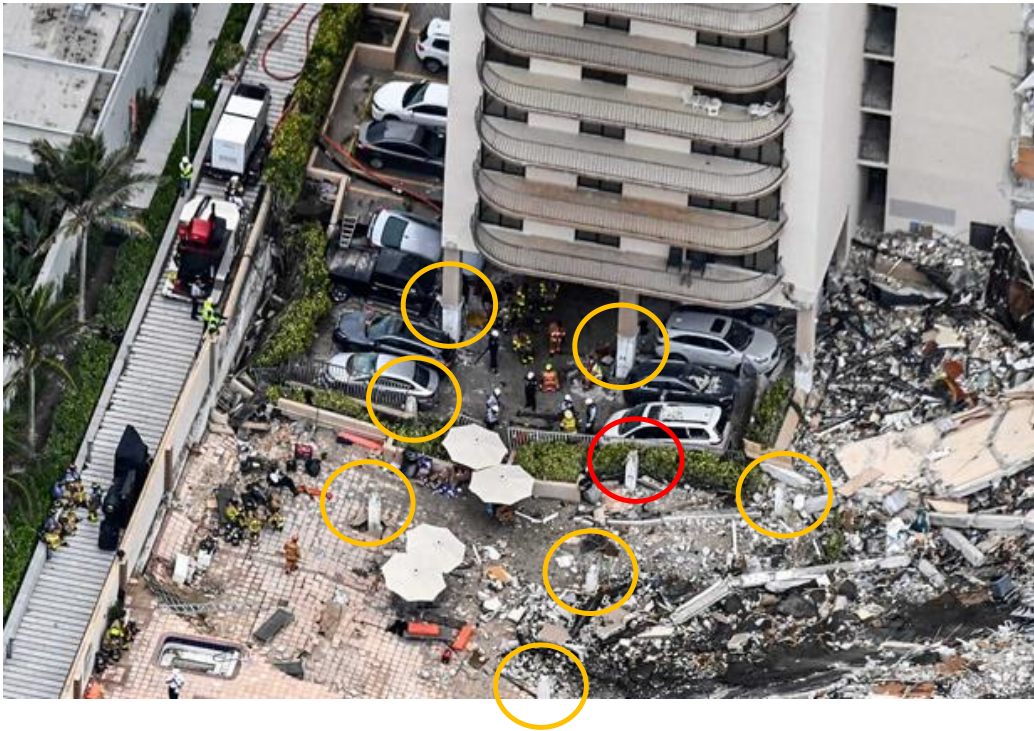
| | Min. Specified (ASTM 615 Gr. 60) | Perimeter Wall (avg.) | Pool Deck (avg.) |
|------------------------------|----------------------------------|-----------------------|------------------|
| Yield – F_y : psi (MPa) | 60,000 (414) | 69,948 (482) | 77,012 (531) |
| Ultimate – F_u : psi (MPa) | 90,000 (621) | 106,814 (736) | 110,300 (760) |
| Elongation (%) | 7-9 depending on bar size | 12.4 | 12.9 |

Findings & Observations

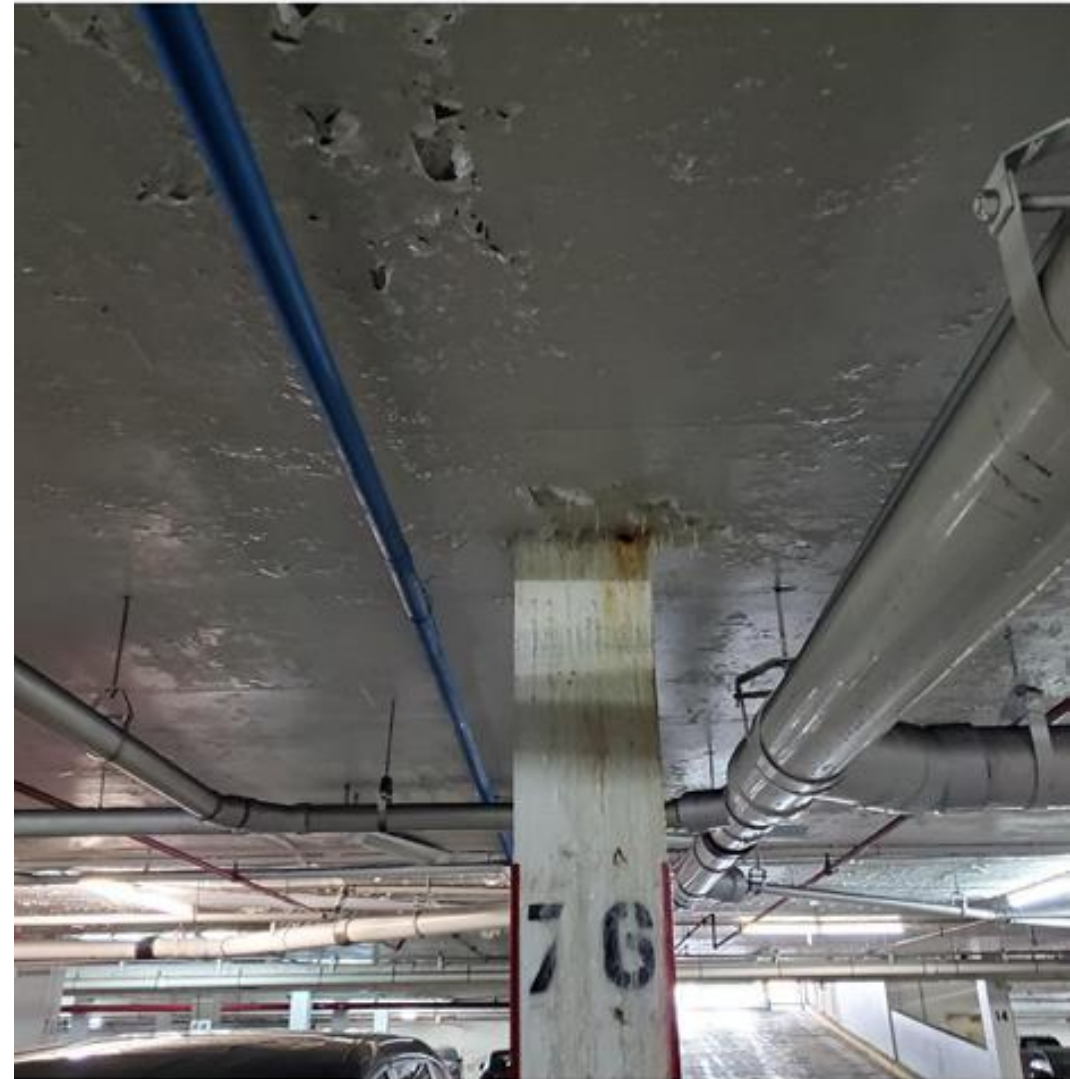
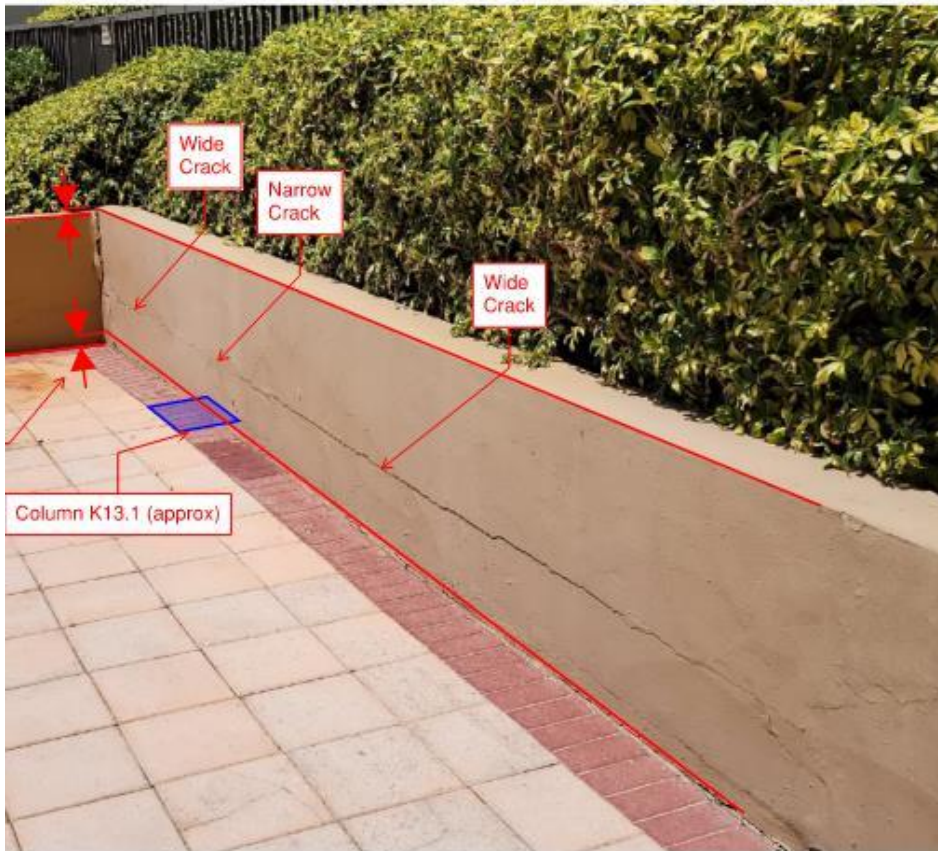
Structural Analysis



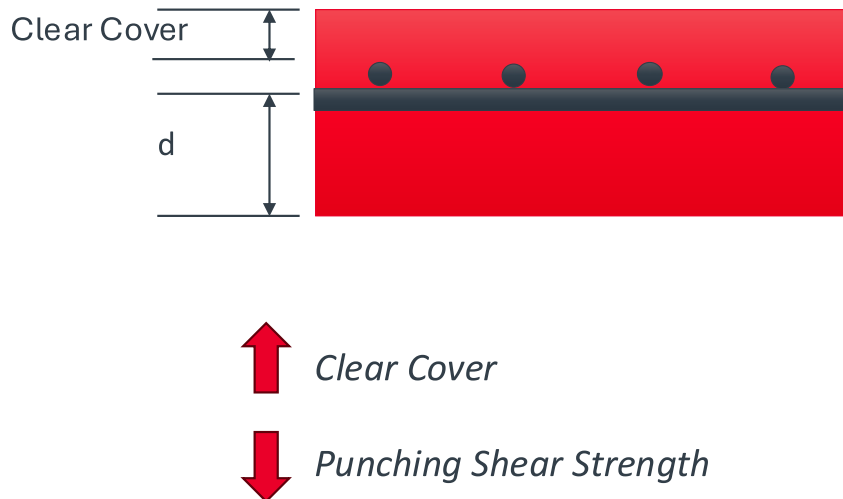
Punching Shear Failures



Pool Deck Slab Distress

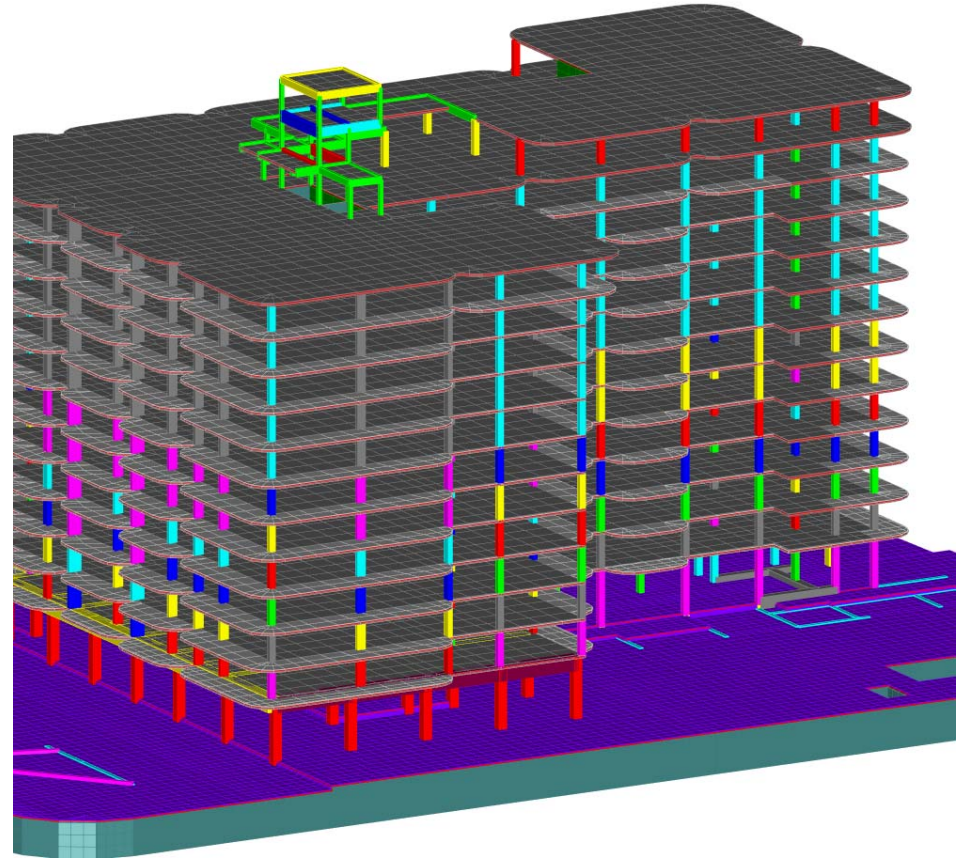
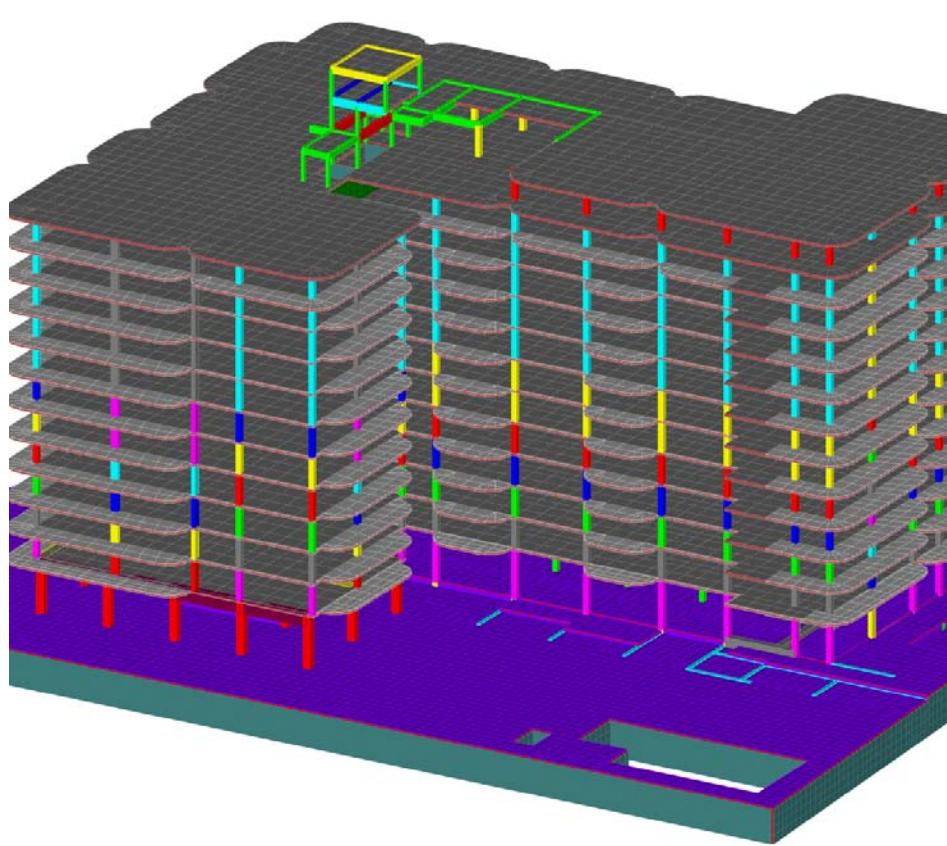


Punching Shear

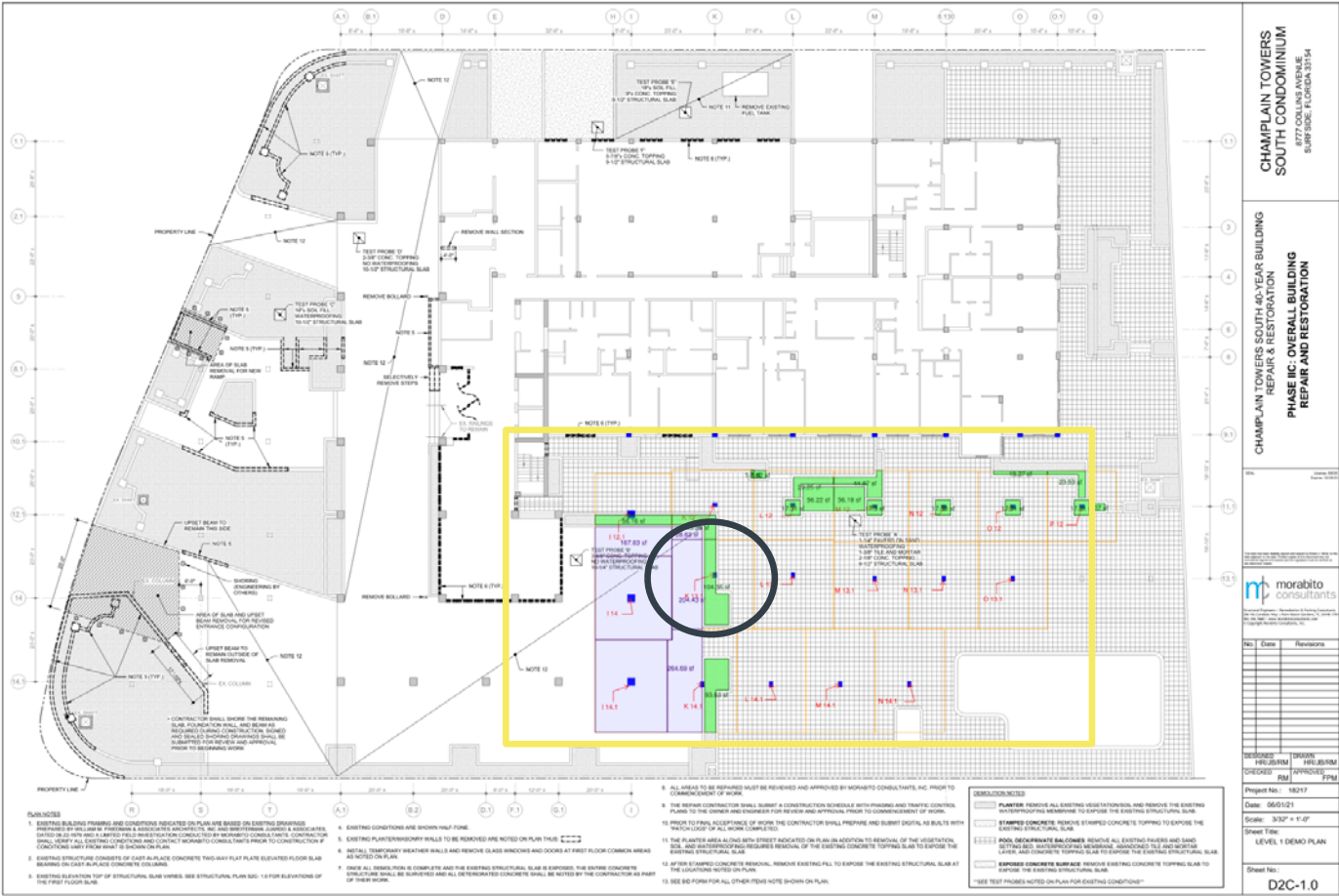


- Punching Shear
 - Dependent on slab depth and concrete strength
 - $V_c = 4\sqrt{f'_c}b_o d$
- Current research shows that:
 - Dependent on flexural reinforcement and slab thickness
 - A coefficient of 4 may be unconservative for low reinforcement ratios

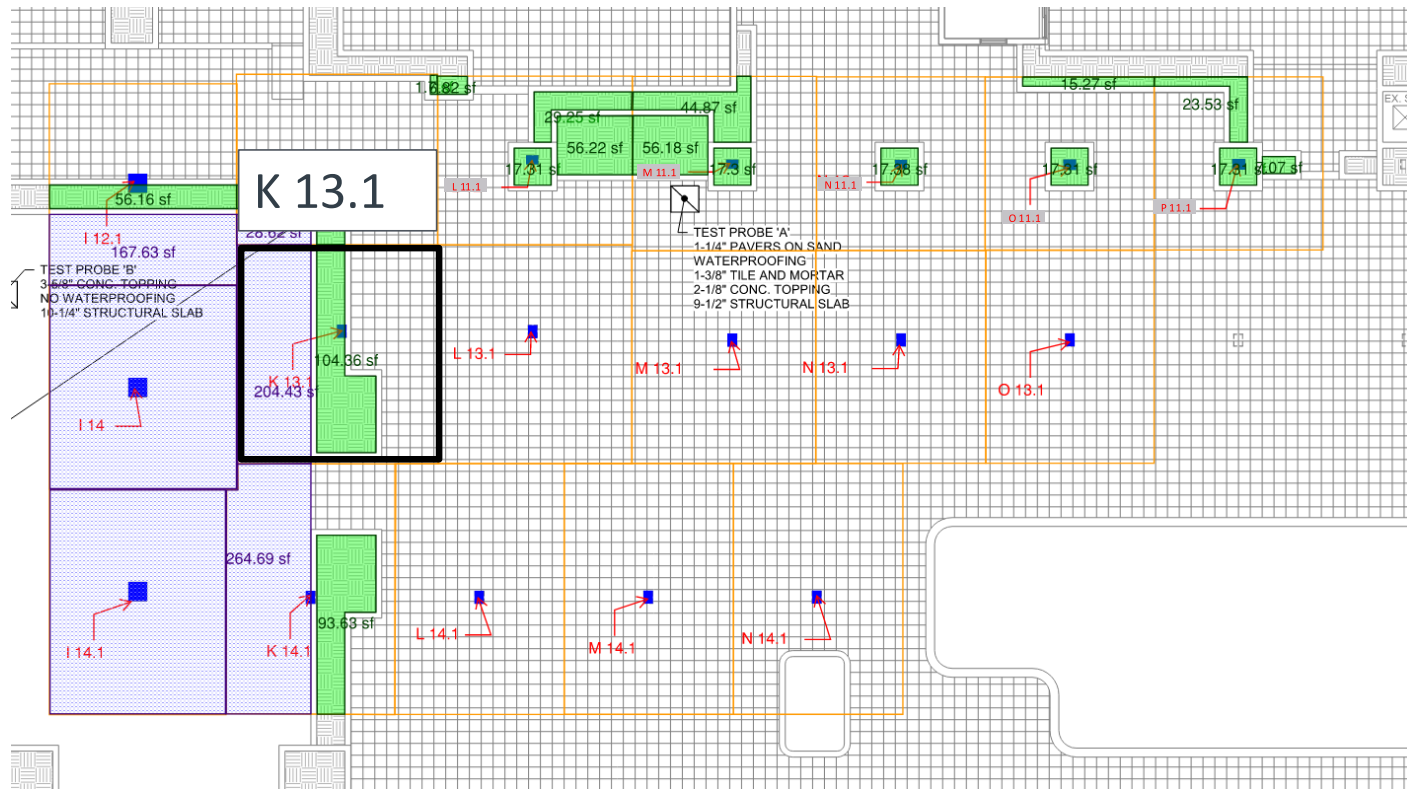
Full Building – Finite Element Model



Pool Deck – At Collapse



Pool Deck – At Collapse



Pool Deck Punching Shear (Column K 13.1)

$$3\sqrt{f'_c}$$

| As Designed (safety factor) | K 13.1 |
|---------------------------------|-------------|
| Size (in x in) | 16x12 |
| Nominal f'_c (psi) | 4000 |
| Clear Cover (in) | 0.75 |
| Factored Load (kip) | 266 |
| Reduced Nominal Capacity (kip) | 155 |
| Demand to Capacity Ratio | 1.72 |

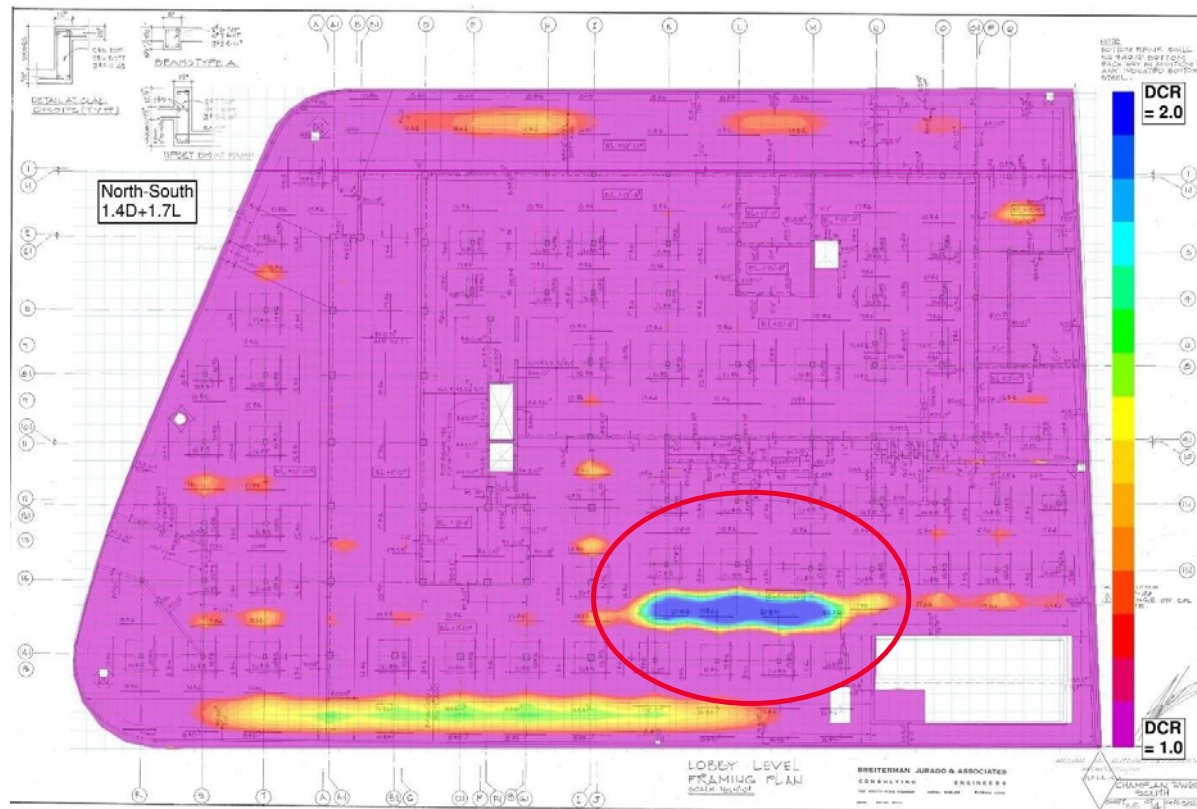
| At Collapse (no safety factor) | K 13.1 |
|---------------------------------|-------------|
| Size (in x in) | 16x12 |
| Estimated f'_c (psi) | 5000 |
| Clear Cover (in) | 2.13 |
| Estimated Load (D) (kip) | 128 |
| Nominal Capacity (kip) | 150 |
| Demand to Capacity Ratio | 0.85 |

Demand to Capacity Ratio > 1 = **BAD**

Demand to Capacity Ratio < 1 = **GOOD**

Lobby Level Slab – Finite Element Model

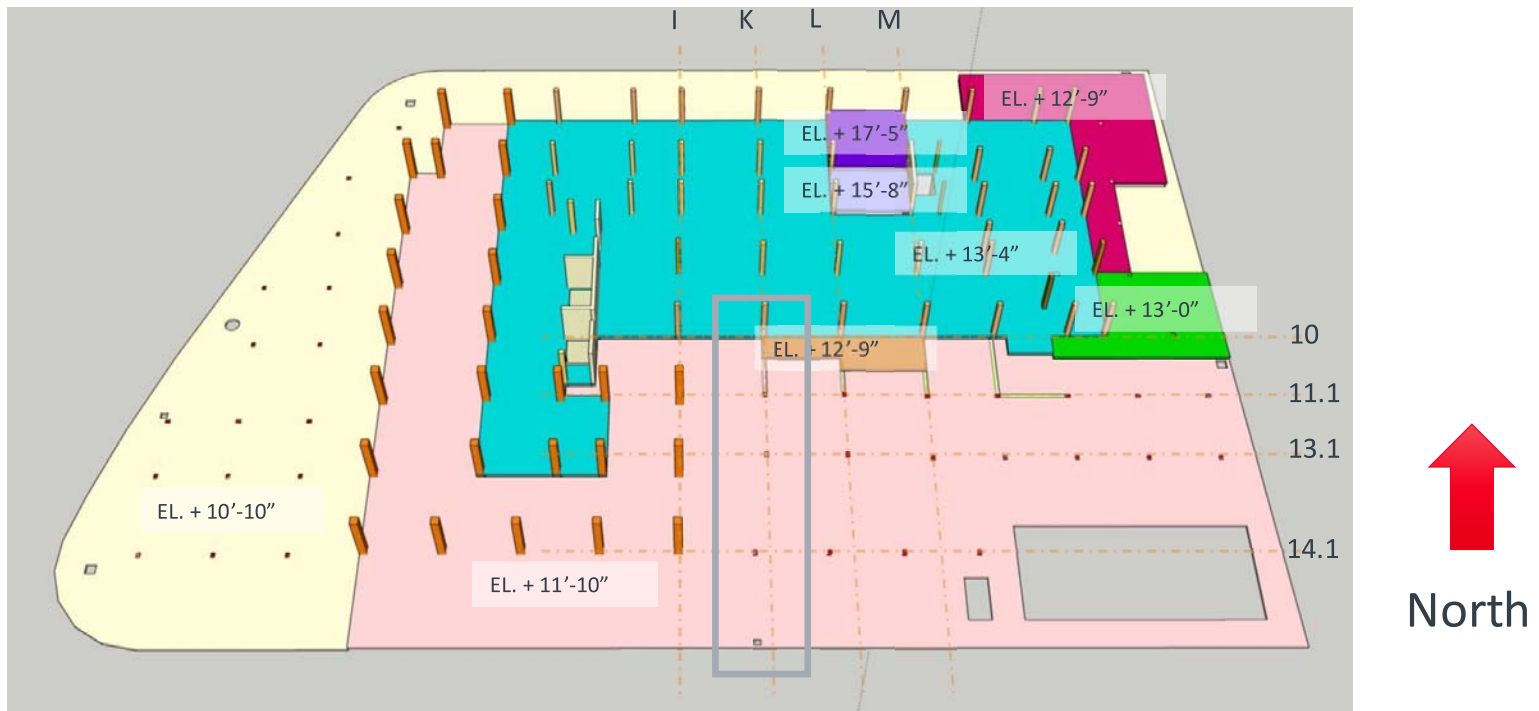
As-Designed Positive Bending, $1.4D+1.7L$, $\Phi = 0.85$



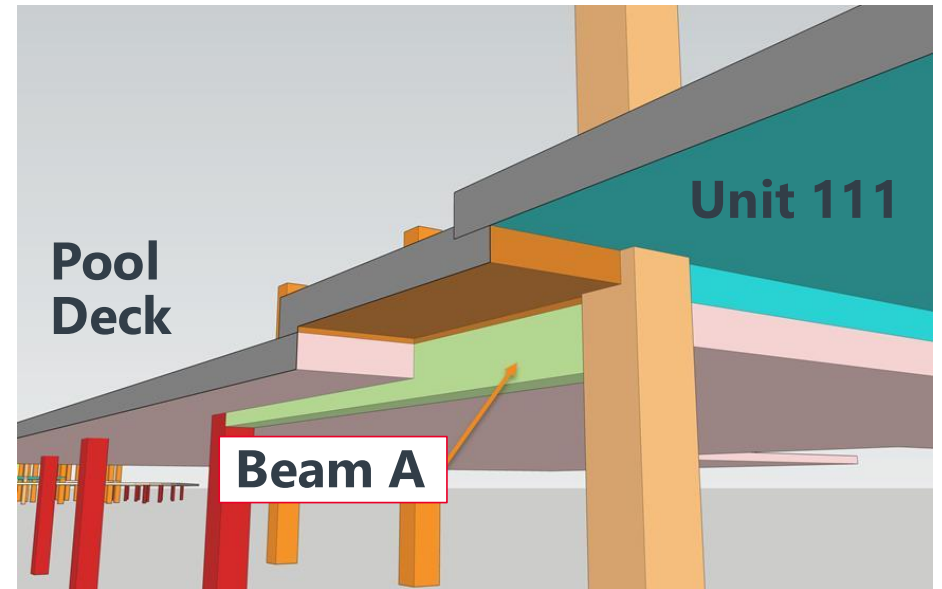
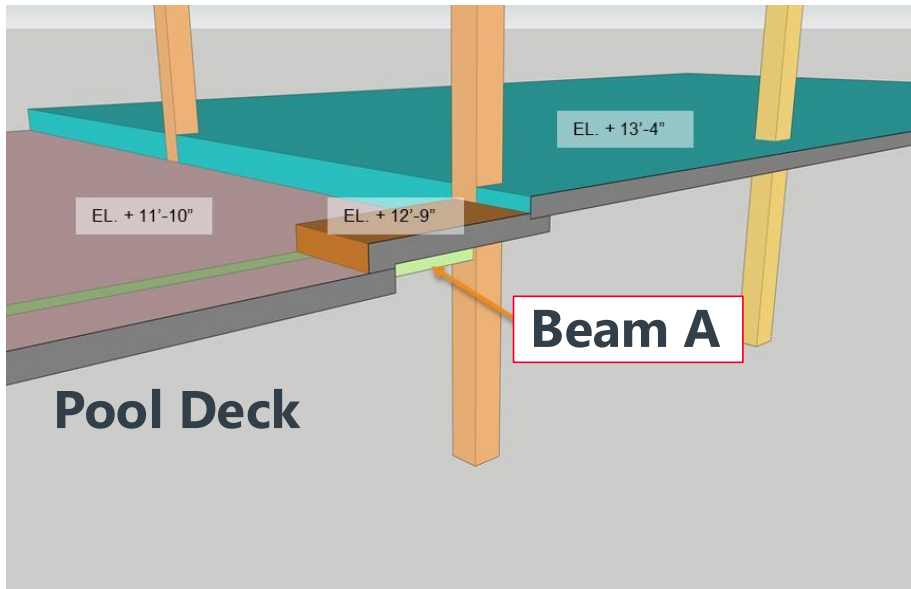
Collapse Theory



Pool Deck/Lobby Level

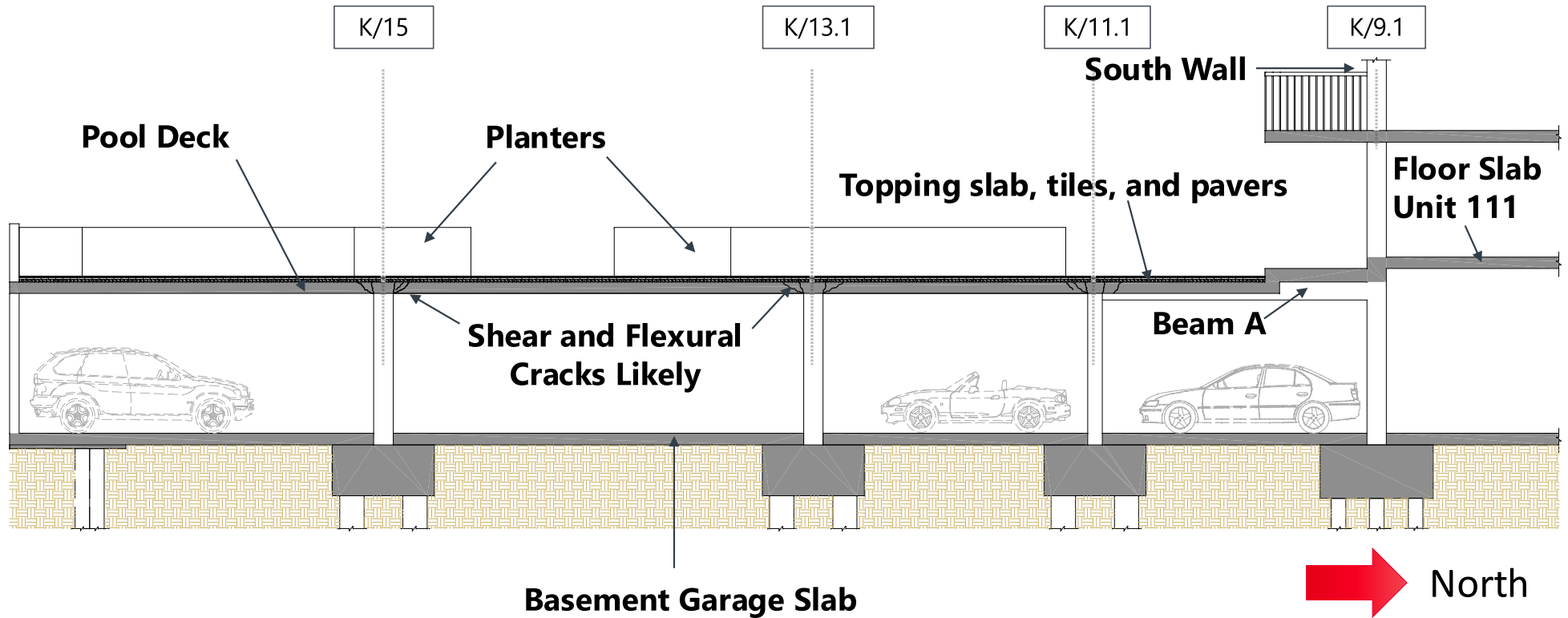


Slab Elevations



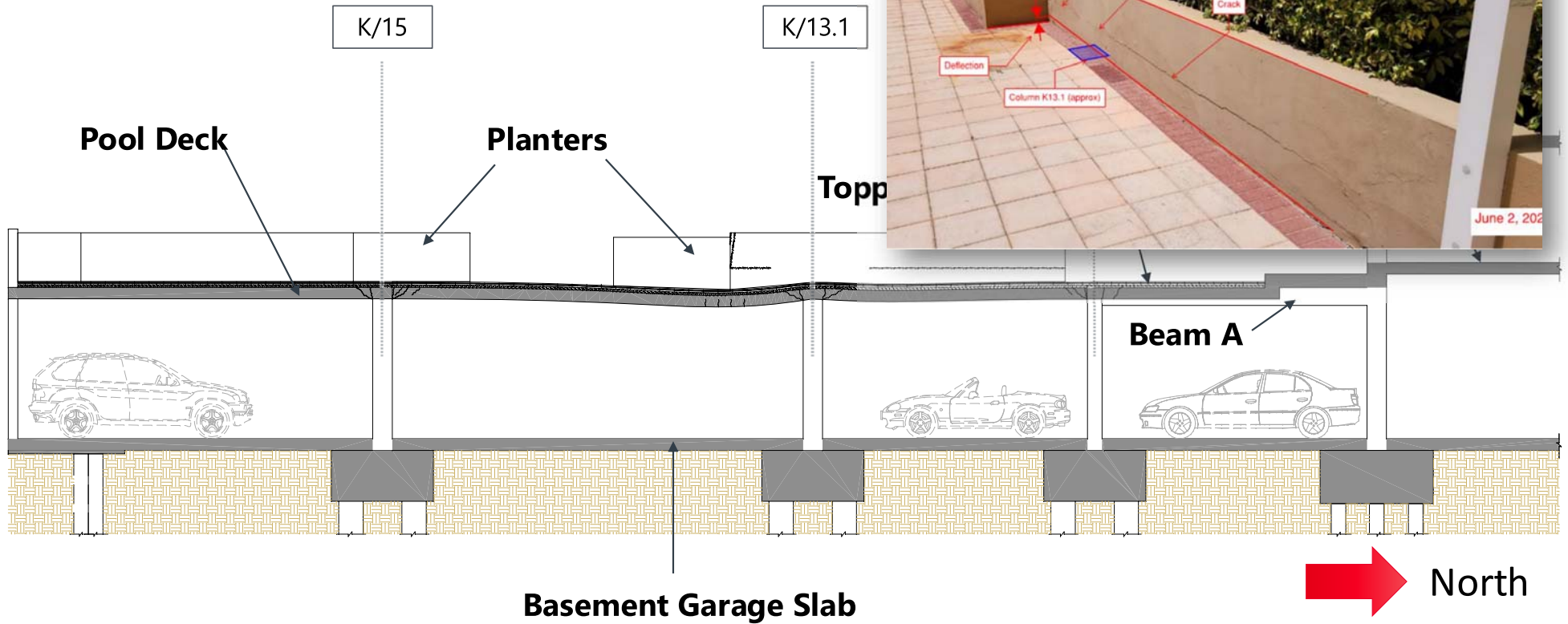
Collapse Hypothesis

Before April 13, 2020



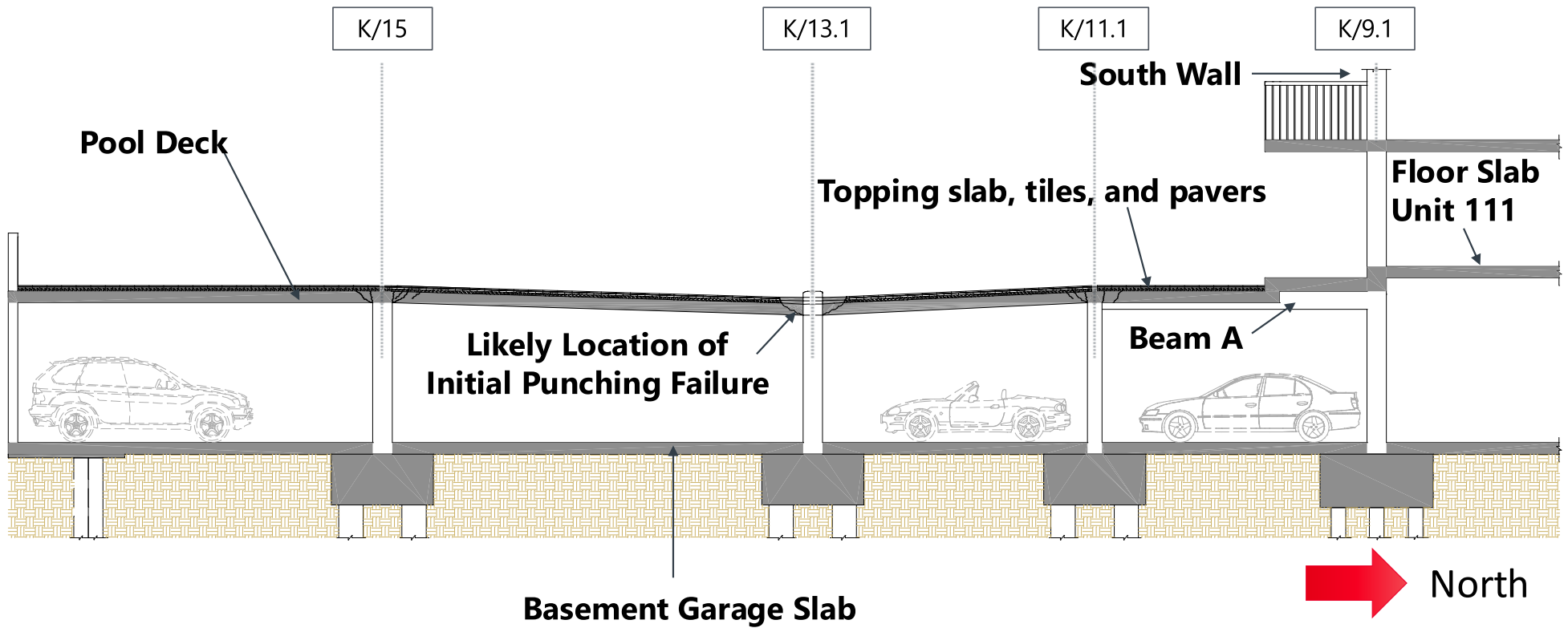
Collapse Hypothesis

After April 13, 2020 and Before June 2, 2021



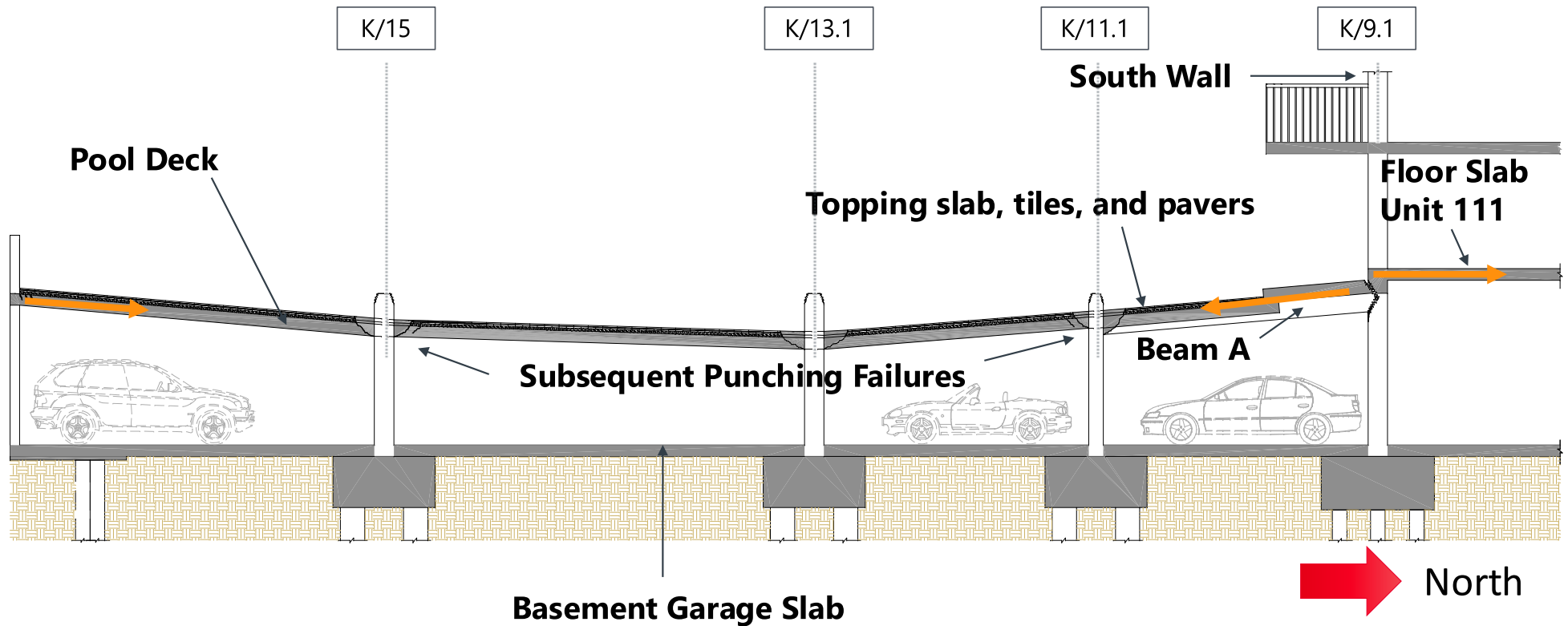
Collapse Hypothesis

June 24, 2021: 1:10 – 1:15 AM



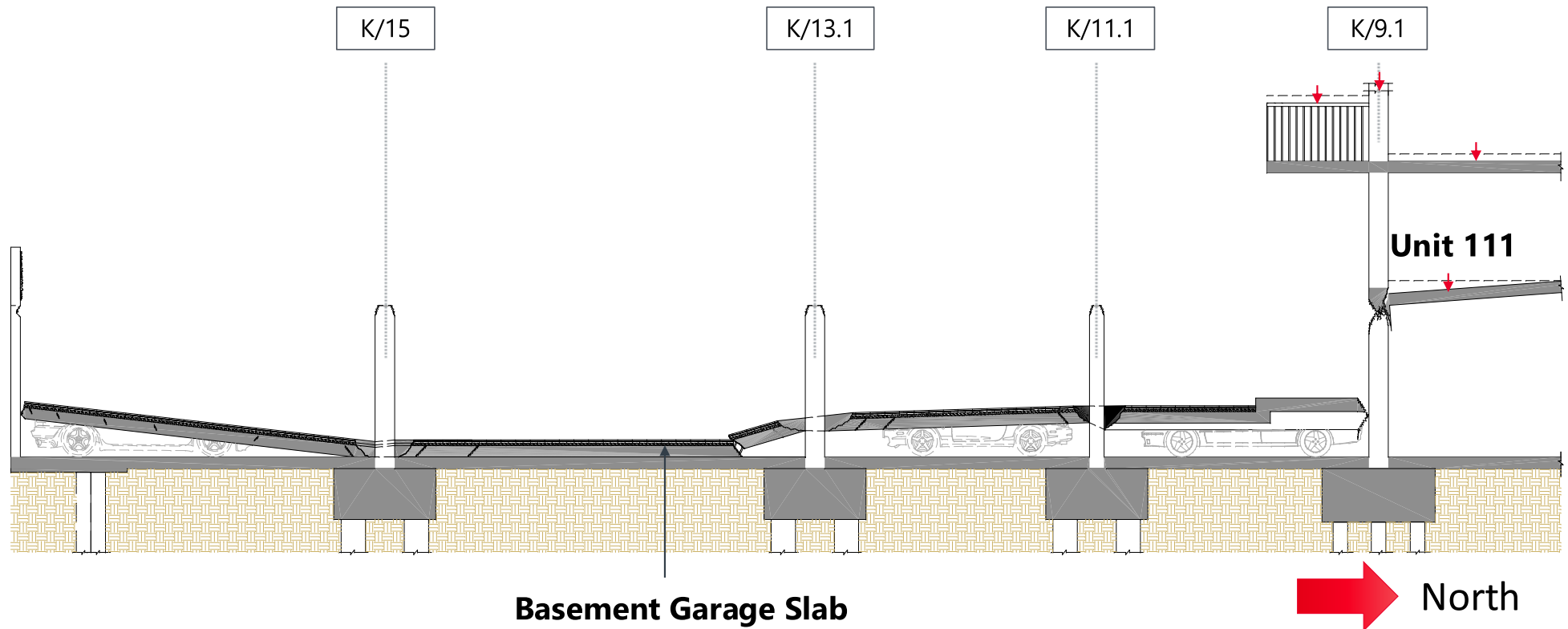
Collapse Hypothesis

June 24, 2021: 1:10 – 1:15 AM

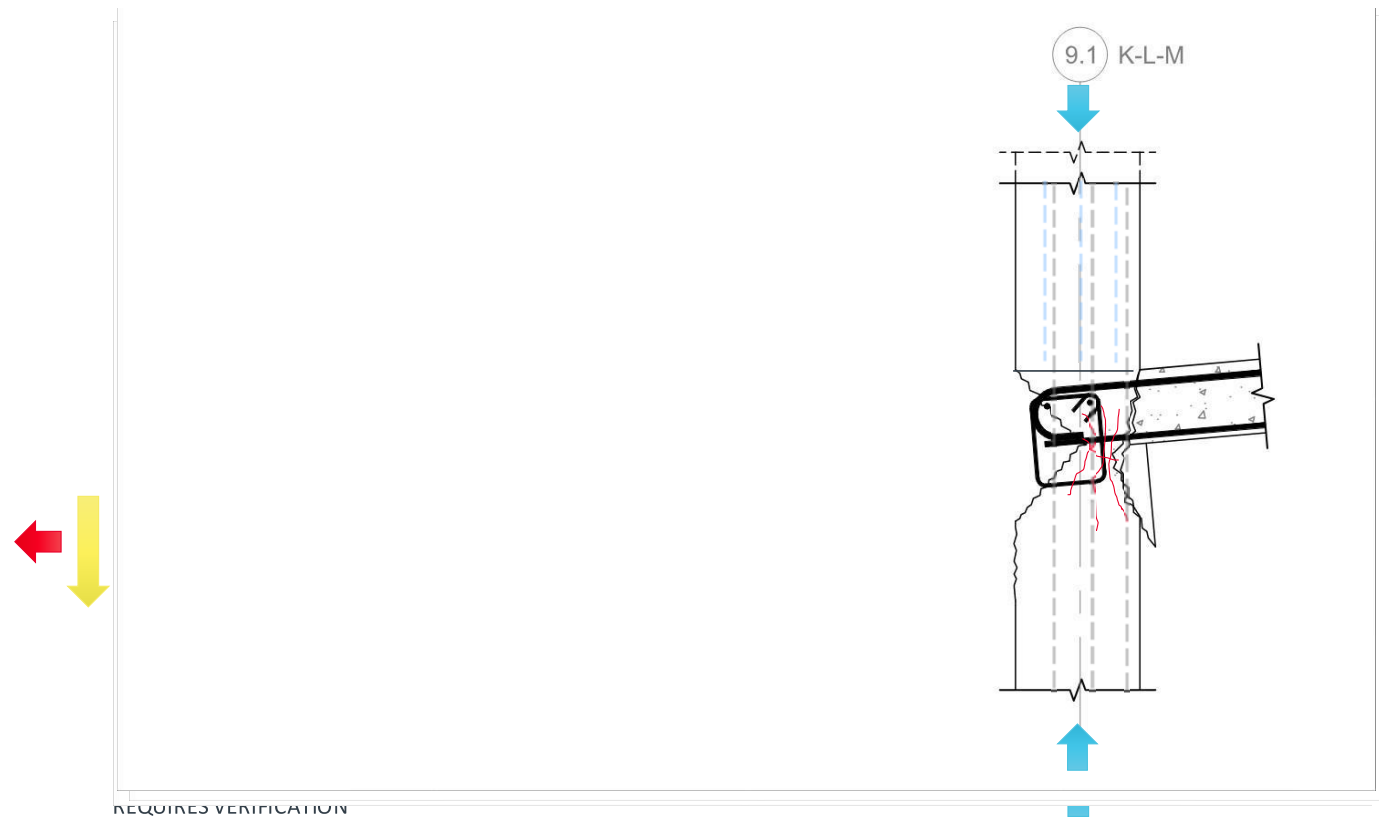


Collapse Hypothesis

June 24, 2021: 1:10 – 1:15 AM

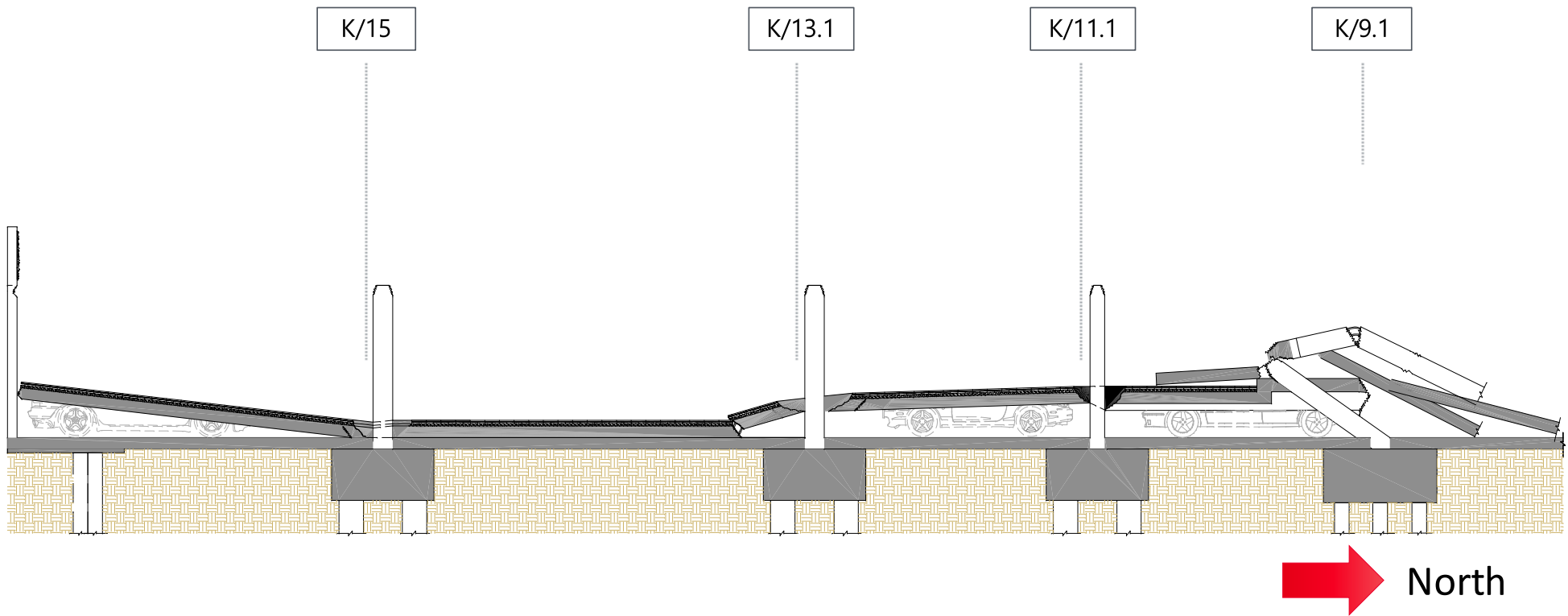


Progressive Collapse Mechanism



Collapse Hypothesis

June 24, 2021: 1:22 AM



Collapse Summary



Mistakes that Appear to have Contributed

Inadequate design of pool deck slab

- Especially punching shear

Excess weight on pool deck

- Original concrete overlay not shown on drawings
- Addition of pavers
- Larger planters than shown on design drawings

Shallow top reinforcement

- Decreasing punching shear strength

Engineers responsible for repairs failed to identify the deficiency

Other Potential Contributing Causes

- Long-term sustained load effects
- Low top flexural reinforcement ratio
 - Code now requires more reinforcement
- Significance unclear
 - Water buildup in planters
 - Corrosion



Judge gives final approval to 'remarkable' \$1 billion Surfside condo collapse settlement

BY LINDA ROBERTSON

UPDATED JUNE 24, 2022 8:48 AM

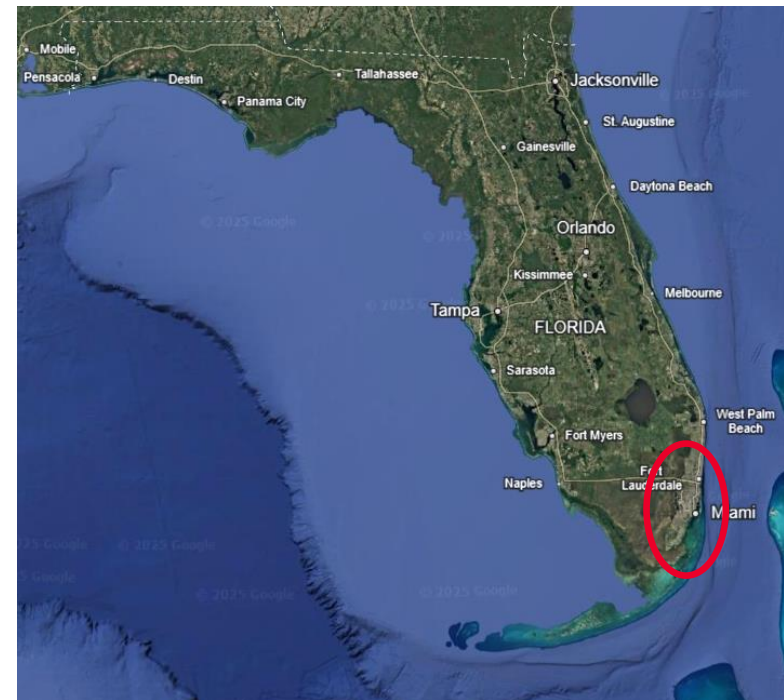


State of Structural Investigations in Florida



Current Status in Florida

- Miami-Dade/Broward have had structural “Recertification”
- After the Champlain Towers South Collapse, Statewide adoption of “Recertification” (SB-4D and SB 154)
- Affects all condominiums 3 stories and higher
- Thousands of buildings, ~900,000 units over 30 years old



Recertification Requirement

- Inspections are:
 - Prescriptive
 - Visual-only
 - Limited to observable distress
- **Design deficiencies are undetectable without distress manifestation**



REGULATORY AND ECONOMIC RESOURCES DEPARTMENT
11805 SW 26th Street, Miami, Florida 33175
786-315-2000
Miami-dade.gov/building

MINIMUM INSPECTION PROCEDURAL GUIDELINES FOR BUILDING STRUCTURAL RECERTIFICATION

| | |
|------------------------|----------------|
| CASE REFERENCE NUMBER: | LICENSEE NAME: |
| | TITLE: |
| JURISDICTION NAME: | ADDRESS: |
| | SIGNATURE: |

*Use separate sheets for additional responses by referencing the report number.

| | |
|---|--|
| 1. DESCRIPTION OF BUILDING | |
| a. Name on Title: | |
| b. Building Street Address: | Bldg. #: |
| c. Legal Description: | Attached: <input type="checkbox"/> |
| d. Owner's Name: | |
| e. Owner's Mailing Address: | |
| f. Folio Number of Property on which Building is Located: | |
| g. Building Code Occupancy Classification: | |
| h. Present Use: | |
| i. General Description of building (overall description, structural systems, special features): | |
| | |
| | |
| j. Number of Stories: | k. Is this a Threshold Building as per 553.71(12) F.S. (Yes/No): |
| l. Provide an aerial of the property identifying the building being certified on a separate sheet. Attached: <input type="checkbox"/> | |
| m. Additional Comments: | |
| | |
| | |
| | |

Most Importantly

- Educate the general public to understand:

Structural Repairs \neq Maintenance

Maintenance = Best Practice

- No practical assessment can certify that a building is free of structural deficiencies or “safe”

What is Safe Enough?

Example 1 - Early 1970's Beam With Shear Cracking

- Noted by engineer related to the 50%
 - Already carried concrete repair
 - Original retained
- Engineer's letter building evacuation
 - No analysis or
 - Displacement
- Association structural issue due to prior



Examples 2 - Late 1970s Building With Excessive Column Tie Spacing

- During extensive structural maintenance work related to an ongoing recertification
- Tie spacing in columns was found to be greater than the current code-prescribed minimums
 - Invasive and unsubstantiated investigation
- Engineer drafted a letter recommending conditional occupancy without a proper analysis or understanding of the significance
- Column tie spacing has a minor effect on columns dominated by axial loads (<5% of capacity)



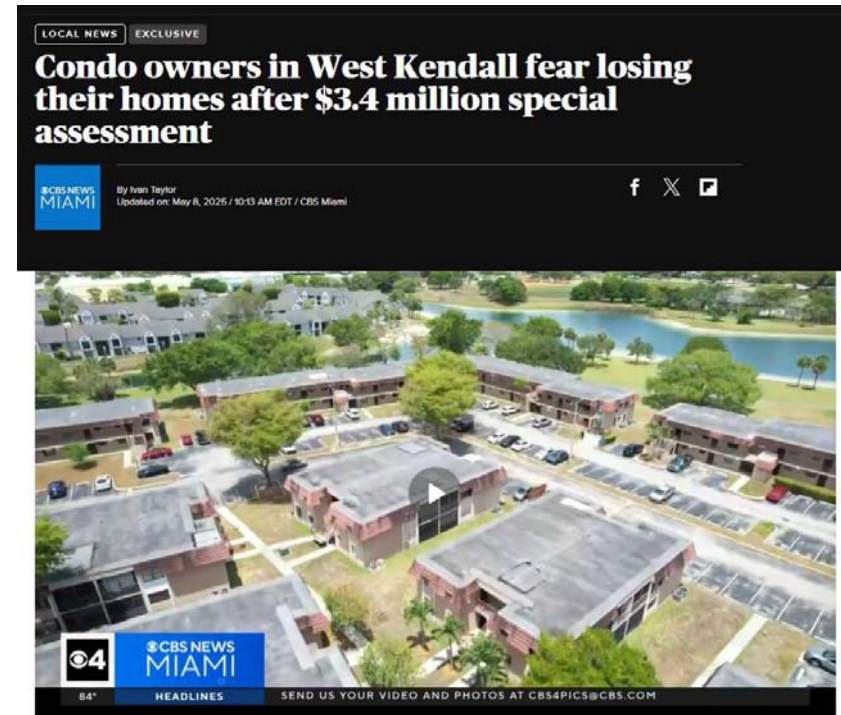
Example 3 – Excessive Maintenance Level Upgrades

- 40-year assessment noted maintenance level distress; the engineer recommend \$ 30 M+ maintenance upgrades
 - No structural deficiencies, laboratory evaluation, or analysis conducted
- Engineers should inform client of options
 - Waterproofing can alter the architectural characteristics
 - Significant upfront costs burden owners
 - Some owners may prefer architectural considerations over maintenance-level performance



We must recognize that engineers:

- Can fail to recognize the significance of observed distress
 - Future standards and guides should promote critical thinking
- Do “drive-by” assessments to get
 - Maintenance-level repairs
 - Construction inspections and administration work
- Owners do not always understand the statutory requirements of the codes/standards
 - Engineers should protect owners from unnecessary and costly repairs
 - Best practice \neq Required
 - Substantiate the need for structural repairs/retrofit appropriately



Champlain Towers Investigation Acknowledgements

- **Akerman LLP:** Michael Goldberg and Brenda Radmacher
- **James River Insurance/Clyde and Co.**
- **Wiss Janney Elstner Associates, Inc.**
 - Gary Klein, PE, SE
- **WJE staff from South Florida and 9 other offices:**
 - Field investigation
 - Document review
 - Structural modeling and review
 - Geotechnical consulting



Thank You

mfadden@walterpmoore.com

786-815-3074